

Influence of Laser Line on Strain Path during Forming of Tailor Welded Blanks

Elliot Biro, PhD, PEng, IWE
University of Waterloo

Project Team

Waterloo Research Team

PhD Student:

Shiyuan Song

PDF Supervisor:

Ahmad Aminzadeh

A/SP Leadership Team

Project Mentor:

Dean Kanelos, Nucor

Team Leads:

Stamping Team - H. Ghassemi-Armaki, GM

Joining Team - L. Huang, GM

Project Leads:

Stamping Team - S. Sheng - GM

Joining Team - T. Zhang - GM

Project Manager:

Eric McCarty, Auto/Steel Partnership

Outline

Introduction

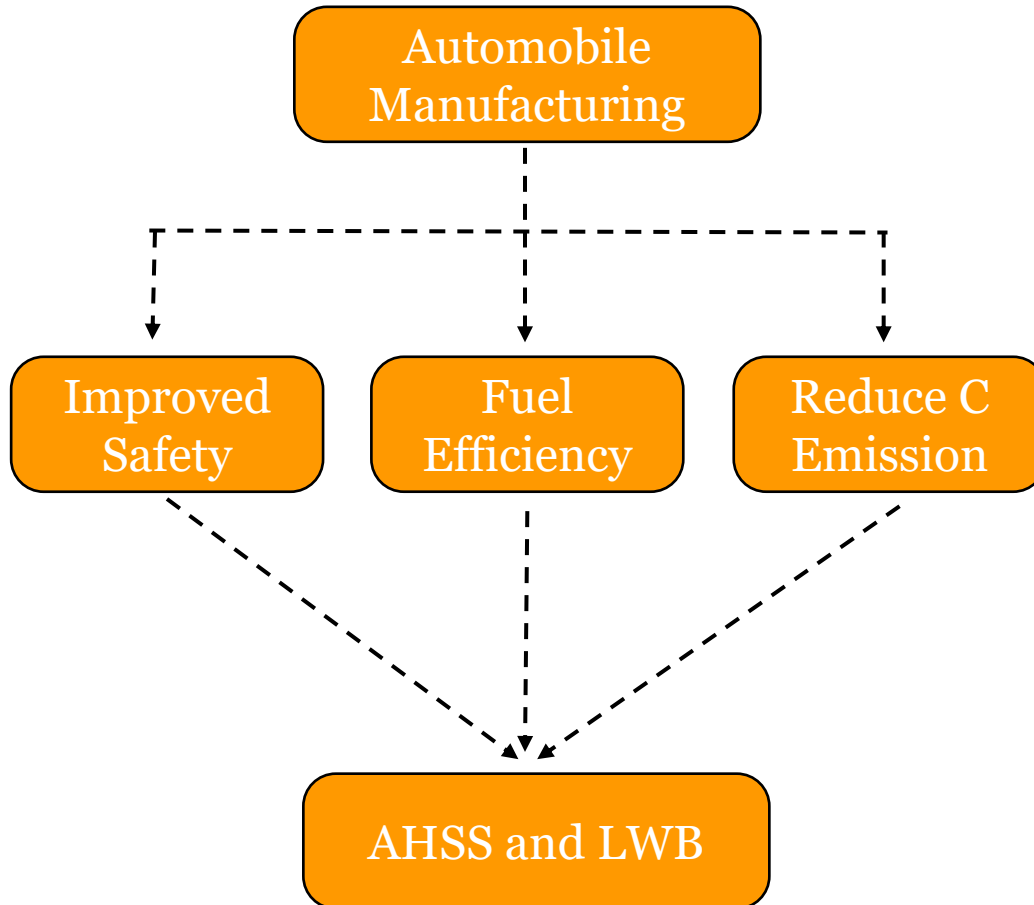
Methodology

Welding Properties

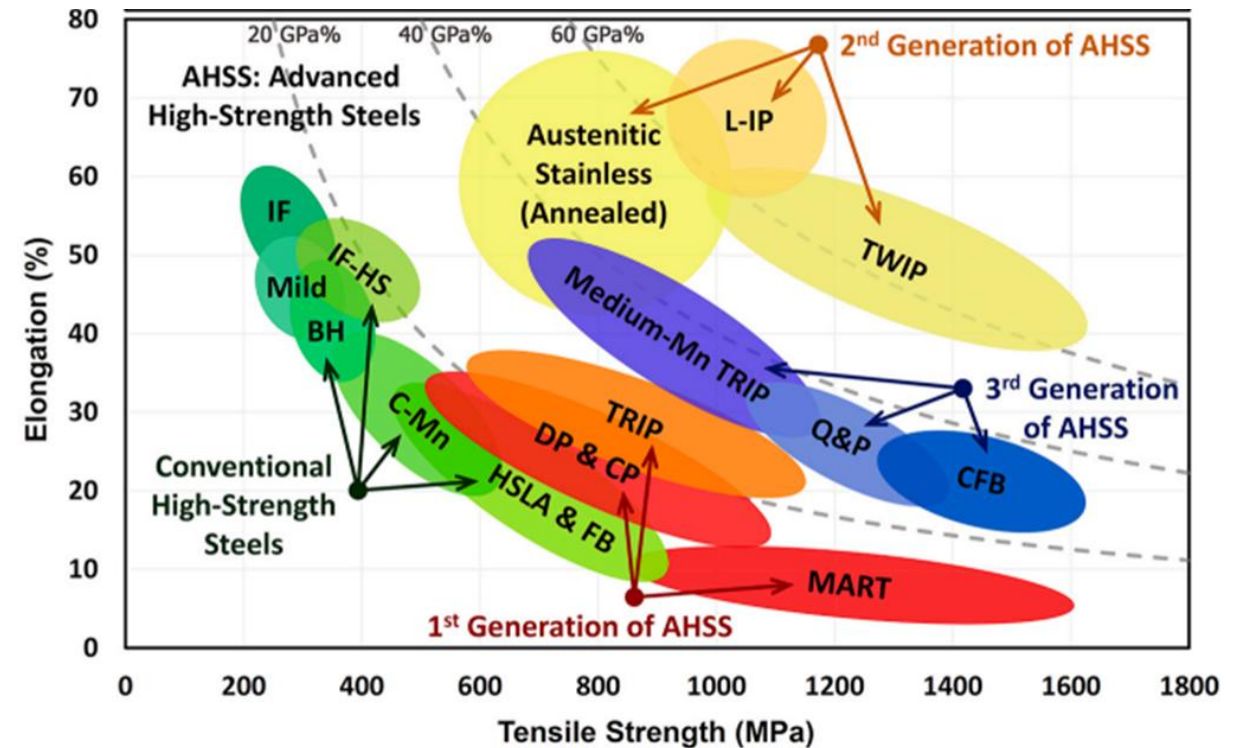
Forming Behavior

Conclusion

Changes in Automotive Construction

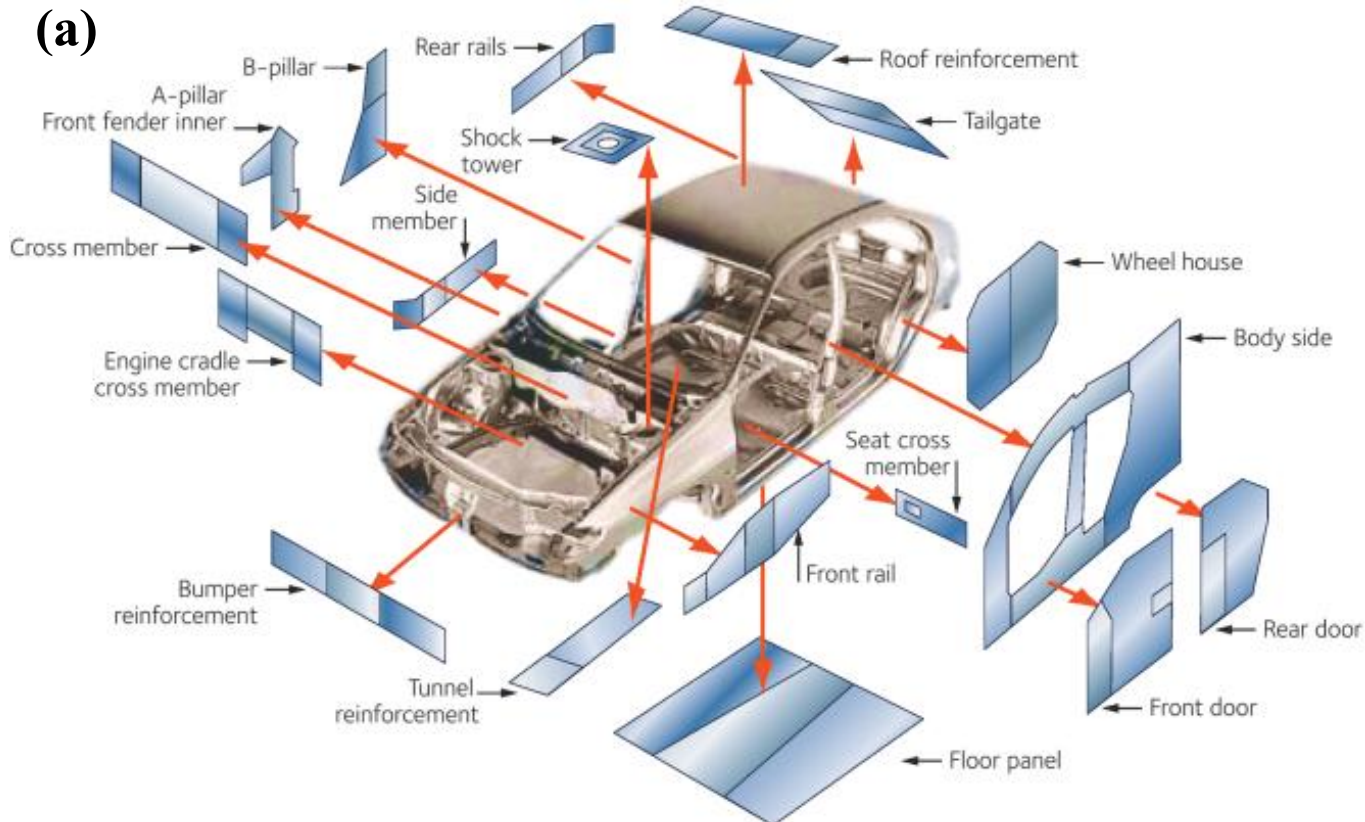


Steel strength ductility diagram
(banana diagram)

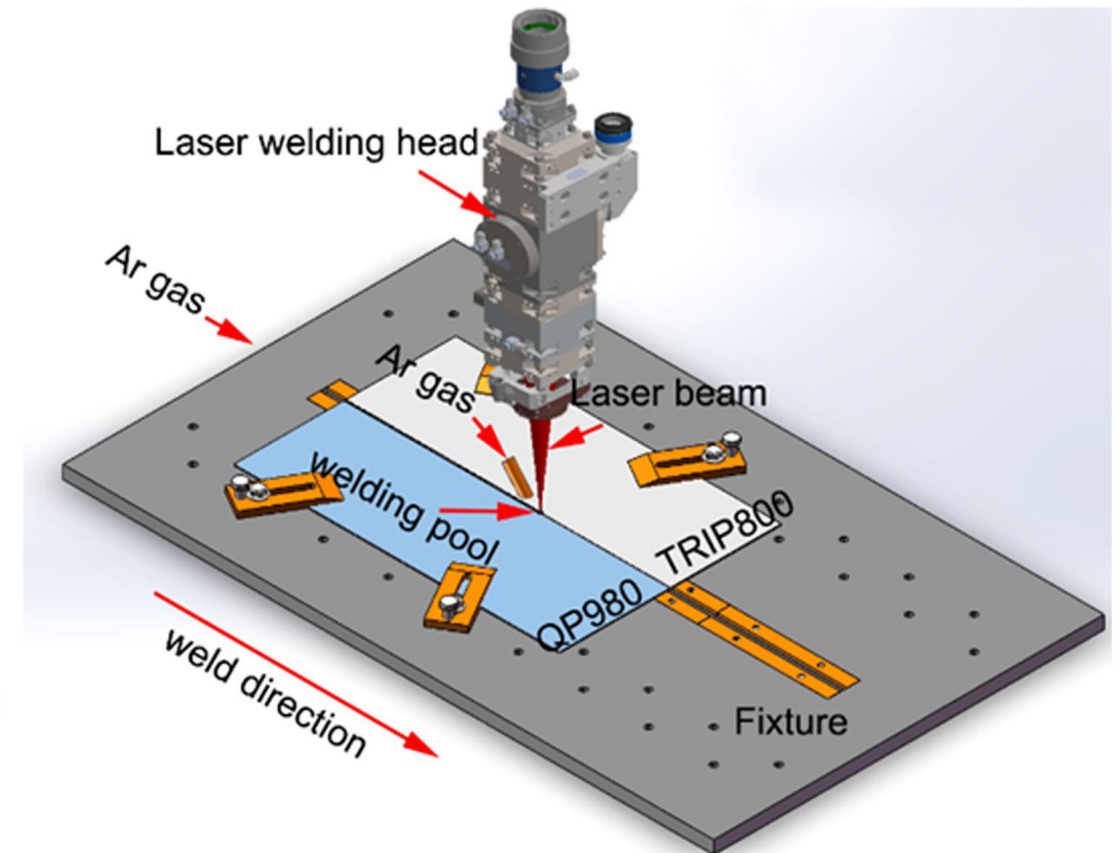


Tailor Welded Blanks

Examples of vehicle components manufactured using laser welded blanks (LWBs)



Laser welding (LW) setups without a filler wire

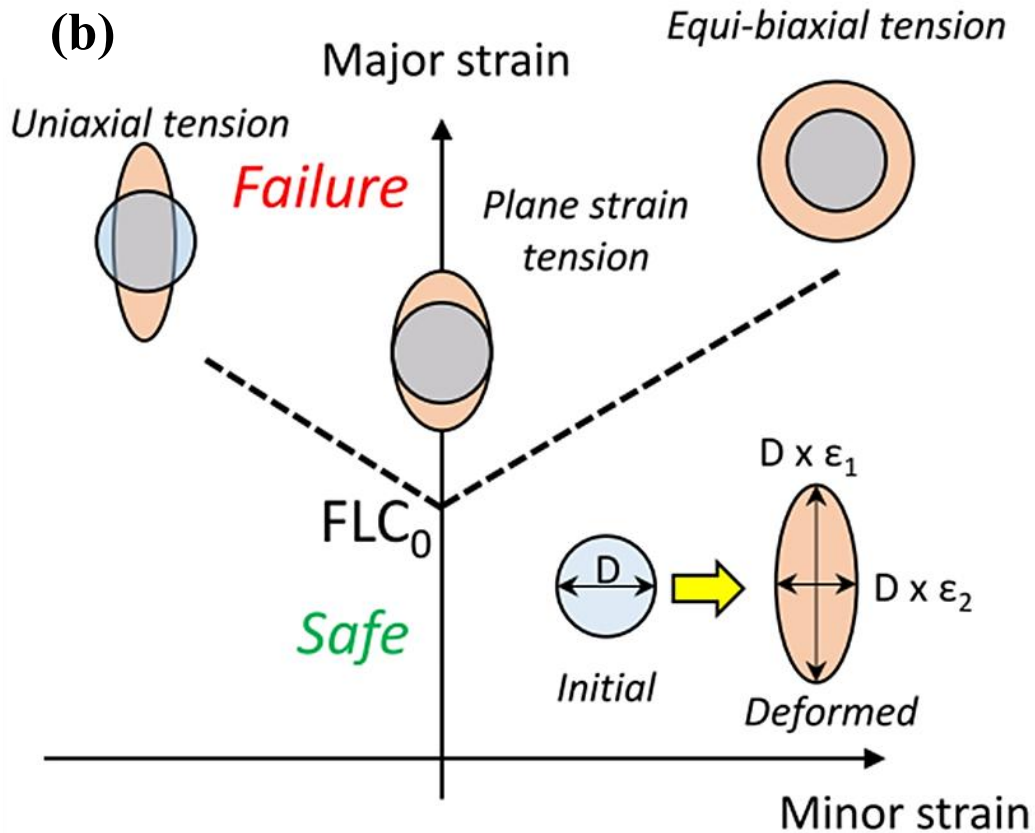


2021_Guo_Investigation on microstructure and properties of dissimilar joint between TRIP800 and QP980 fabricated by laser welding

2023_Öztürk_Investigation of mechanical properties of laser welded dual-phase steels at macro and micro levels

Monolithic Material Formability

- **Nakazima or Marciniak tests (standard):**
Forming limit curves composed of limit strains of materials deformed under uniaxial, plane and biaxial tension states at acute necking or prior to fracture



(a)

Nakazima

Marciniak

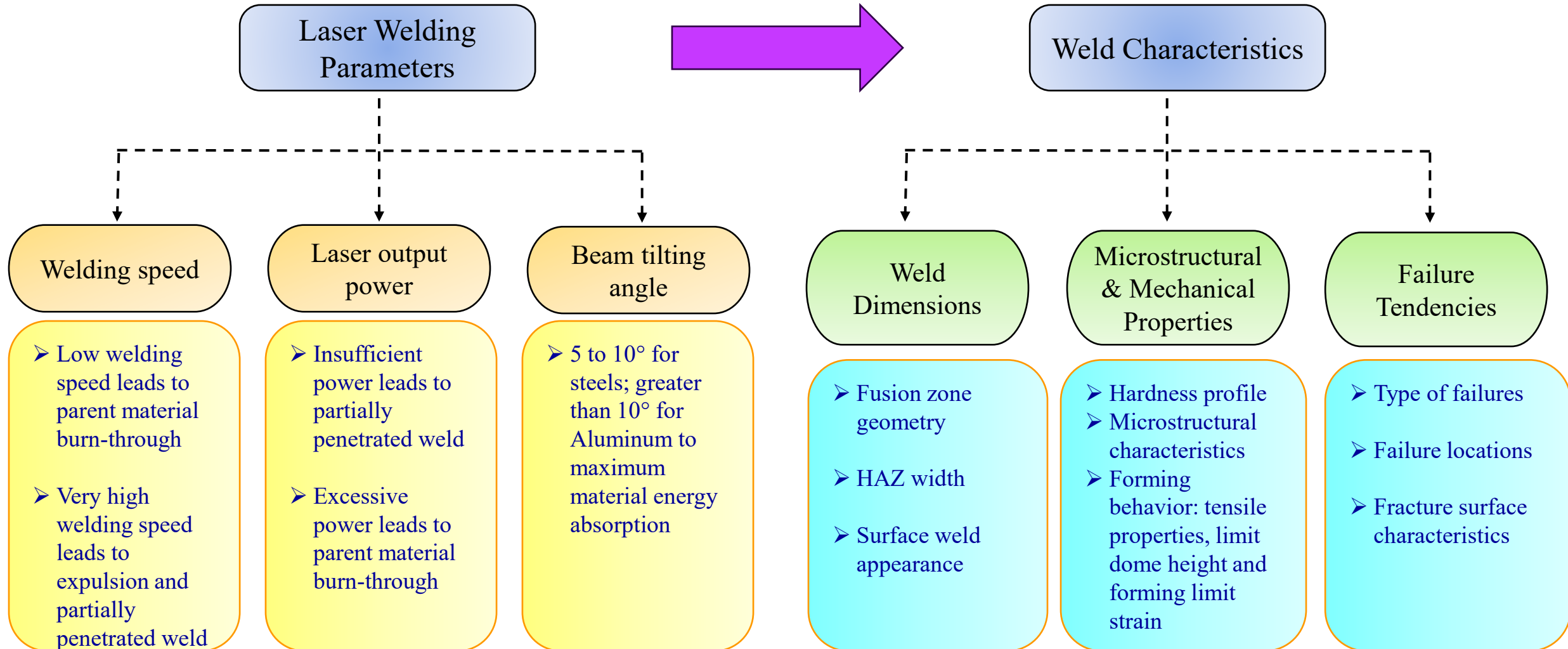


2019_Noder_A comparative investigation into the influence of the constitutive model on the prediction of in-plane formability for Nakazima and Marciniak tests

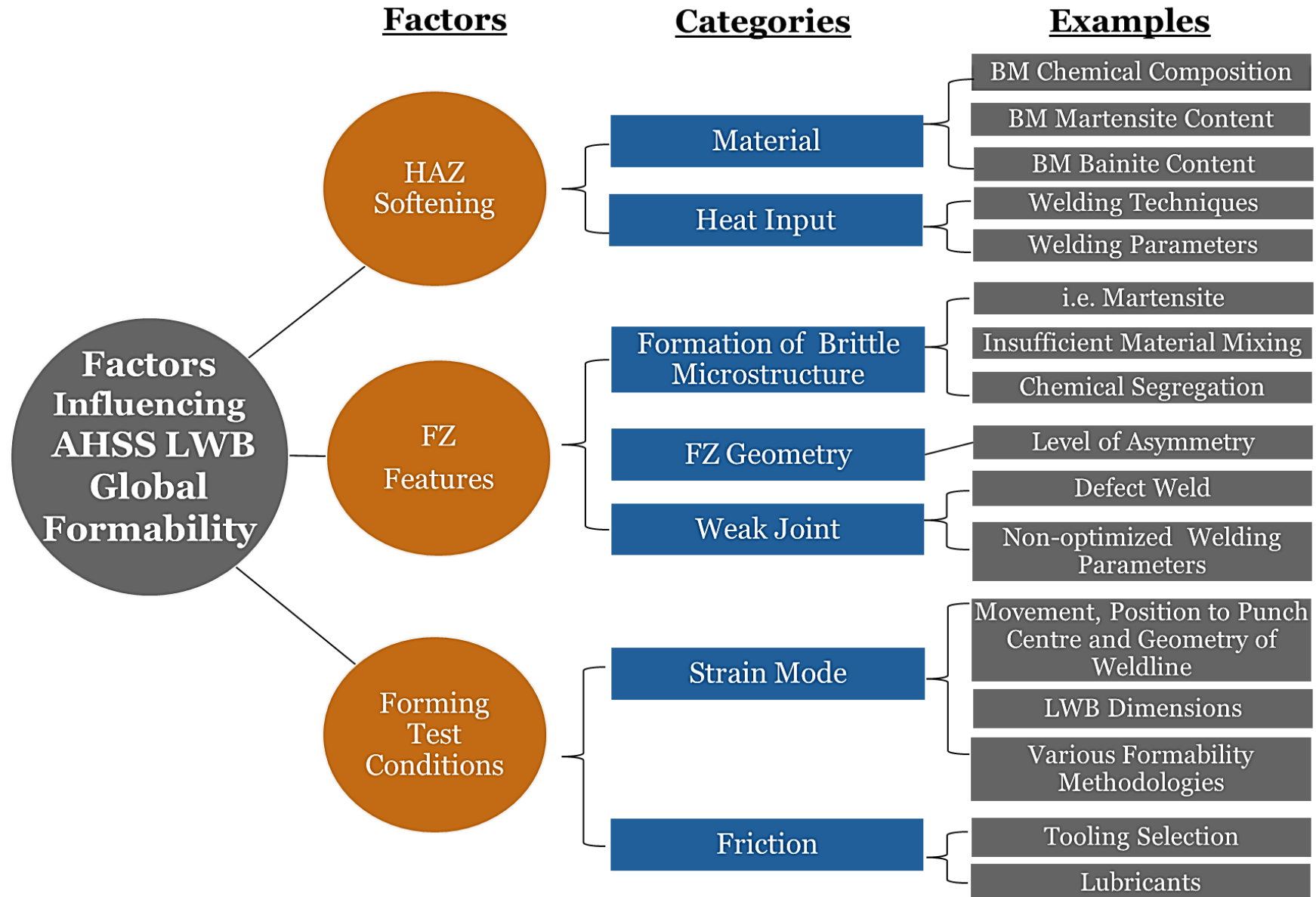
2022_Noder_Plastic Instability and Failure of Sheet Metals Subjected to Complex Stress States

2014_Jasinski_Application of laser speckles to localized necking and cracking detection in Erichsen cupping test

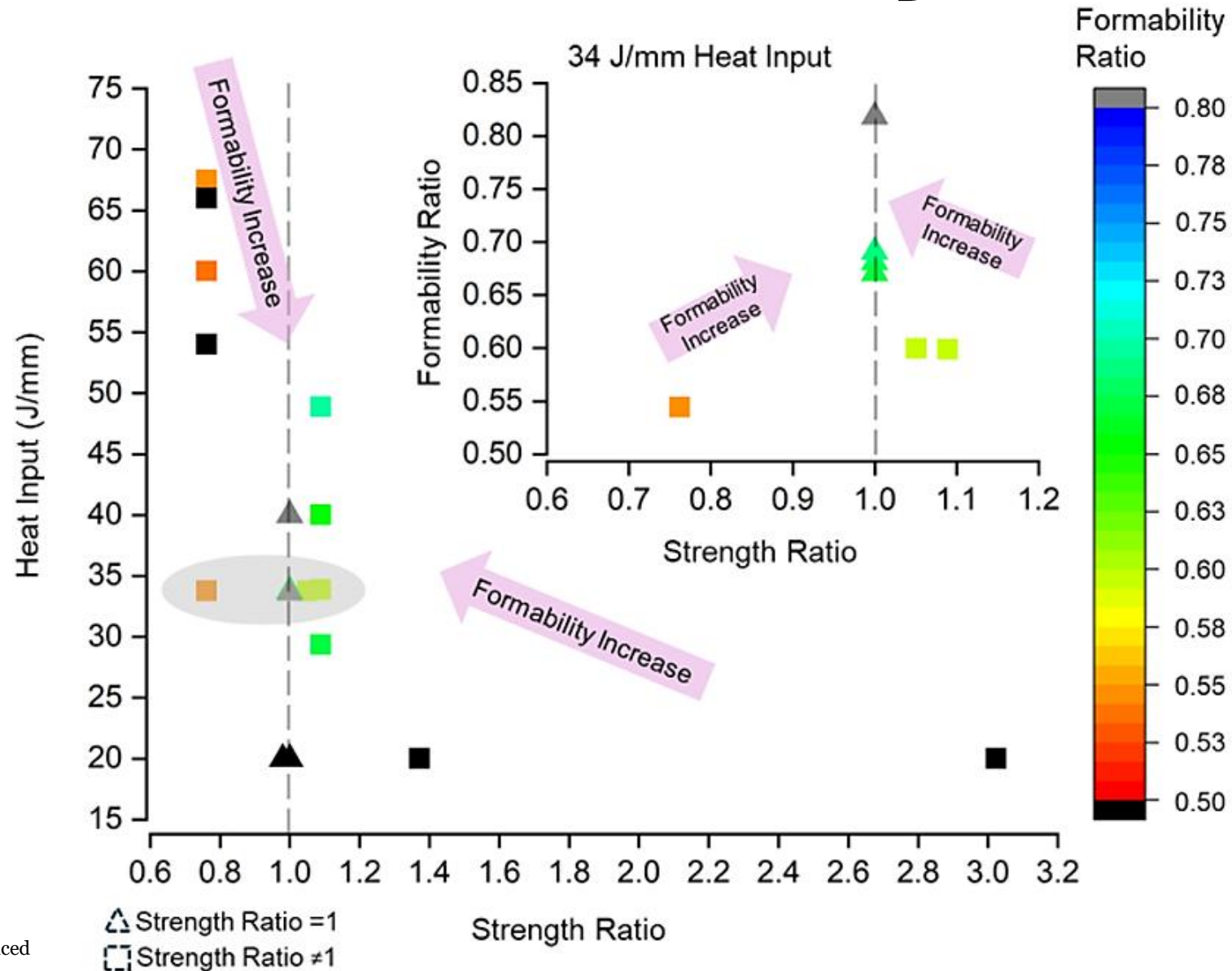
Development of Local Weld Properties



Laser Weld Influence on Formability



Past Results on Laser Blank Formability

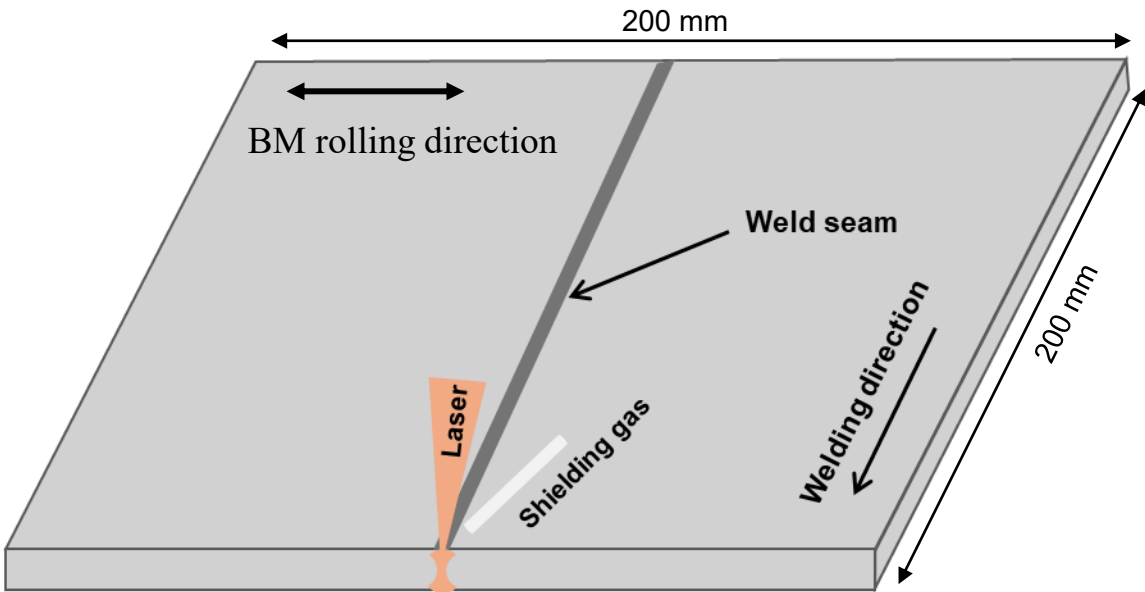
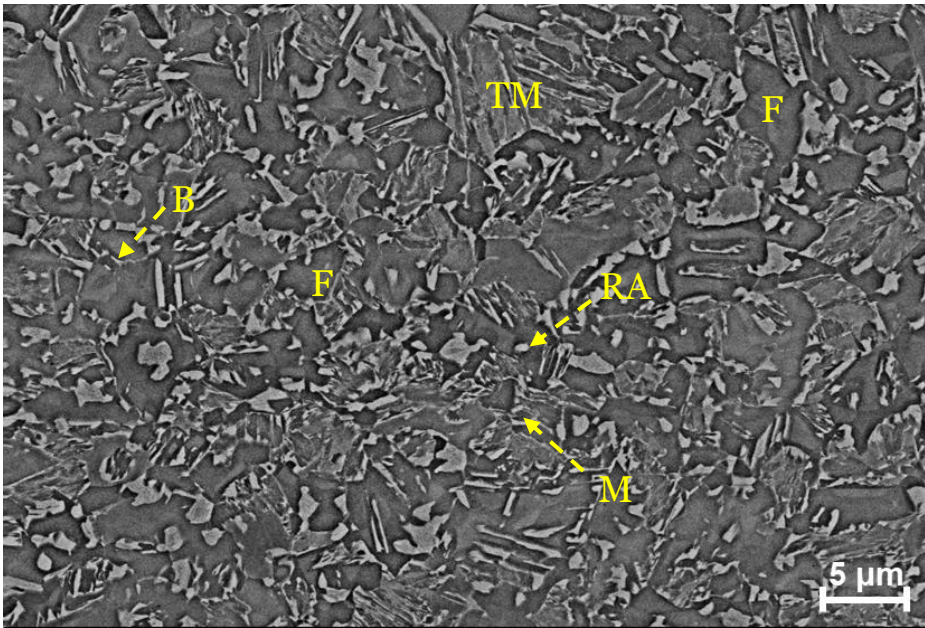


Objectives

How does the presence of the weld line impact the formability of the TWB?

METHODOLOGY

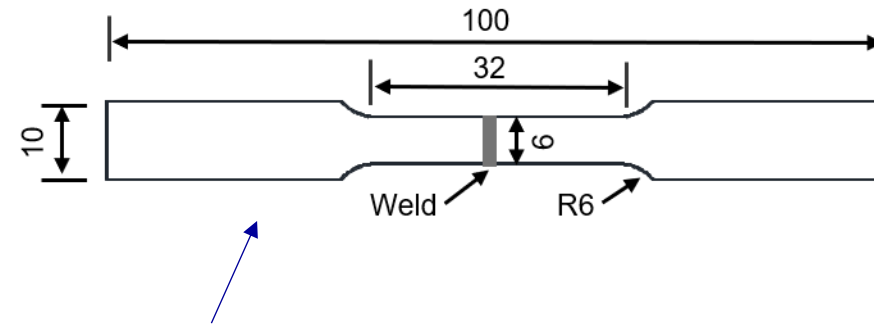
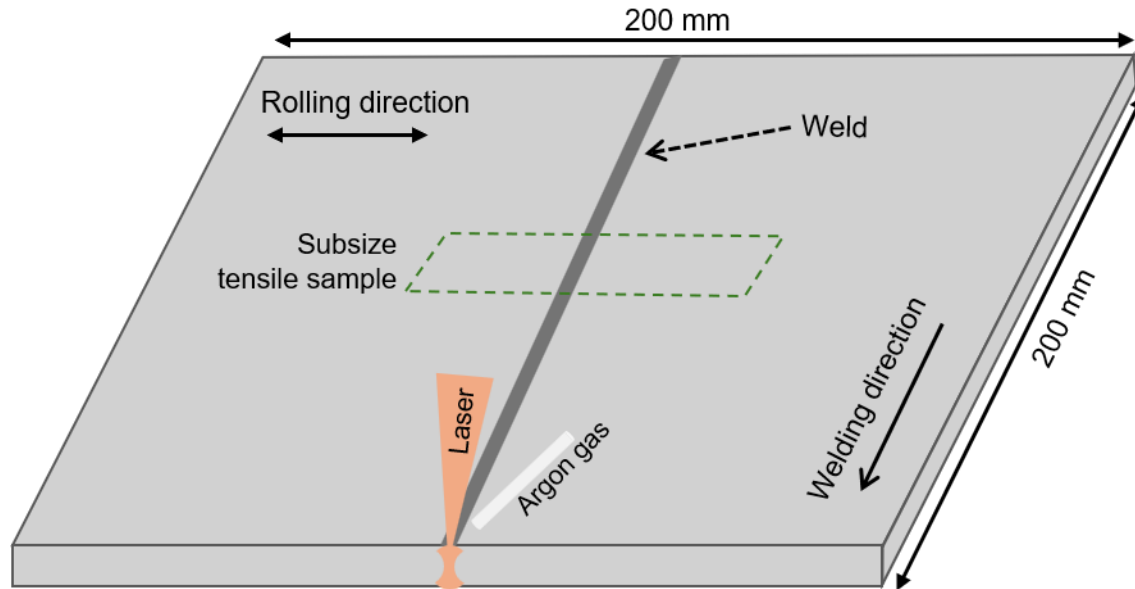
Material and Welding Methodology



Grade	Thickness (mm)	Composition (Wt%)			
		C	Mn+ Si	Cr+ Mo	Nb+ V+Ti
3G-980 GI	1.65	0.22	3.5	0.05	0.007

Top Surface Spot Size (mm)	Power (kW)	Speed	Shielding
0.3 and 1.2	4.5	Varies	Ar

Tensile Testing Geometry

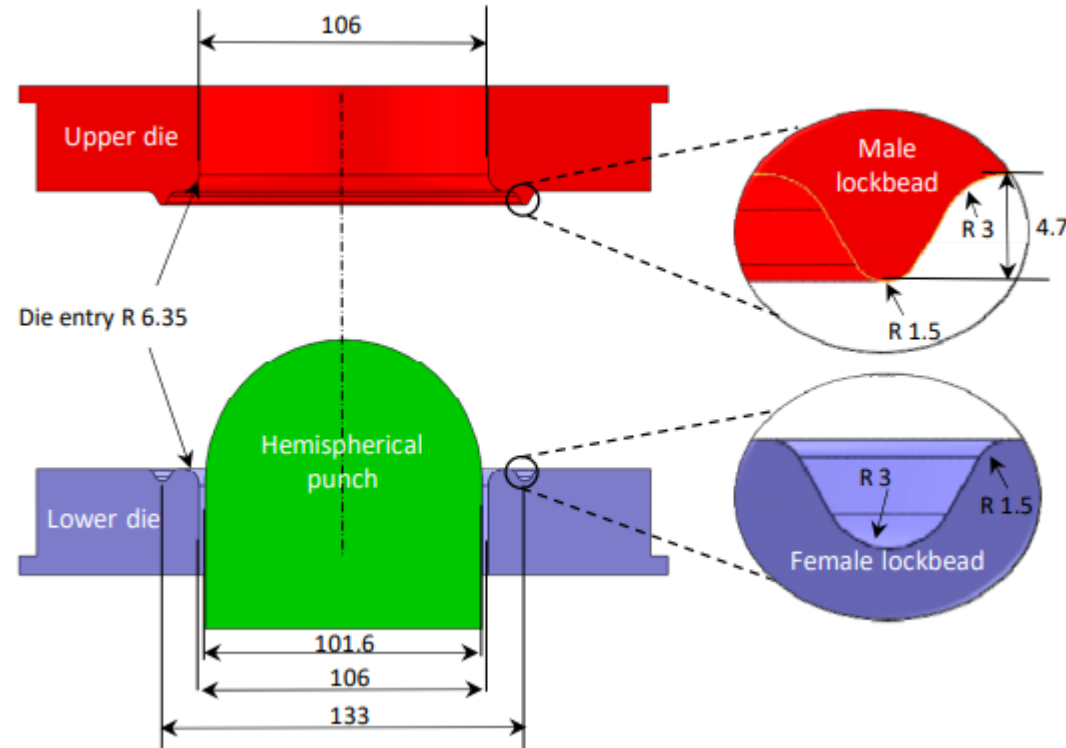


Subsize tensile coupon geometry

- The overall formability of LWBs under uniaxial stretching was evaluated using sub-size tensile specimens.

Forming Test Methodology

Nakazima test tooling

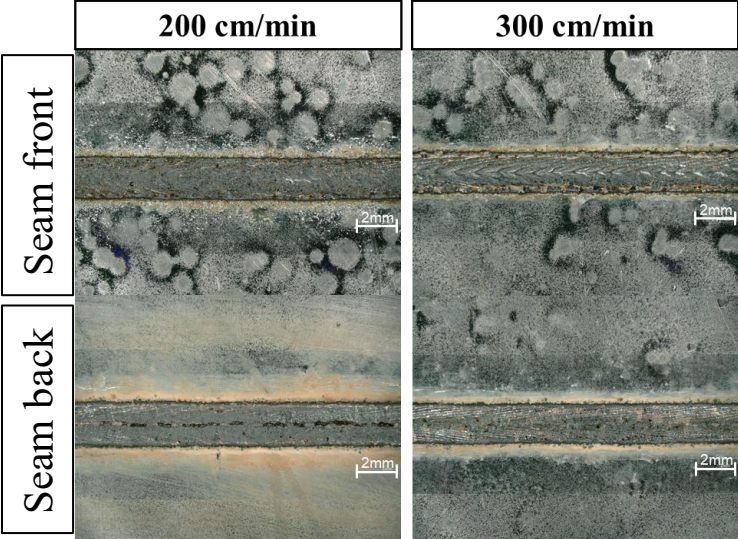


- The Nakazima dome test does not use a carrier blank but a hemispherical punch that deforms the material out-of-plane so that bending, tool contact and non-linear strain paths.

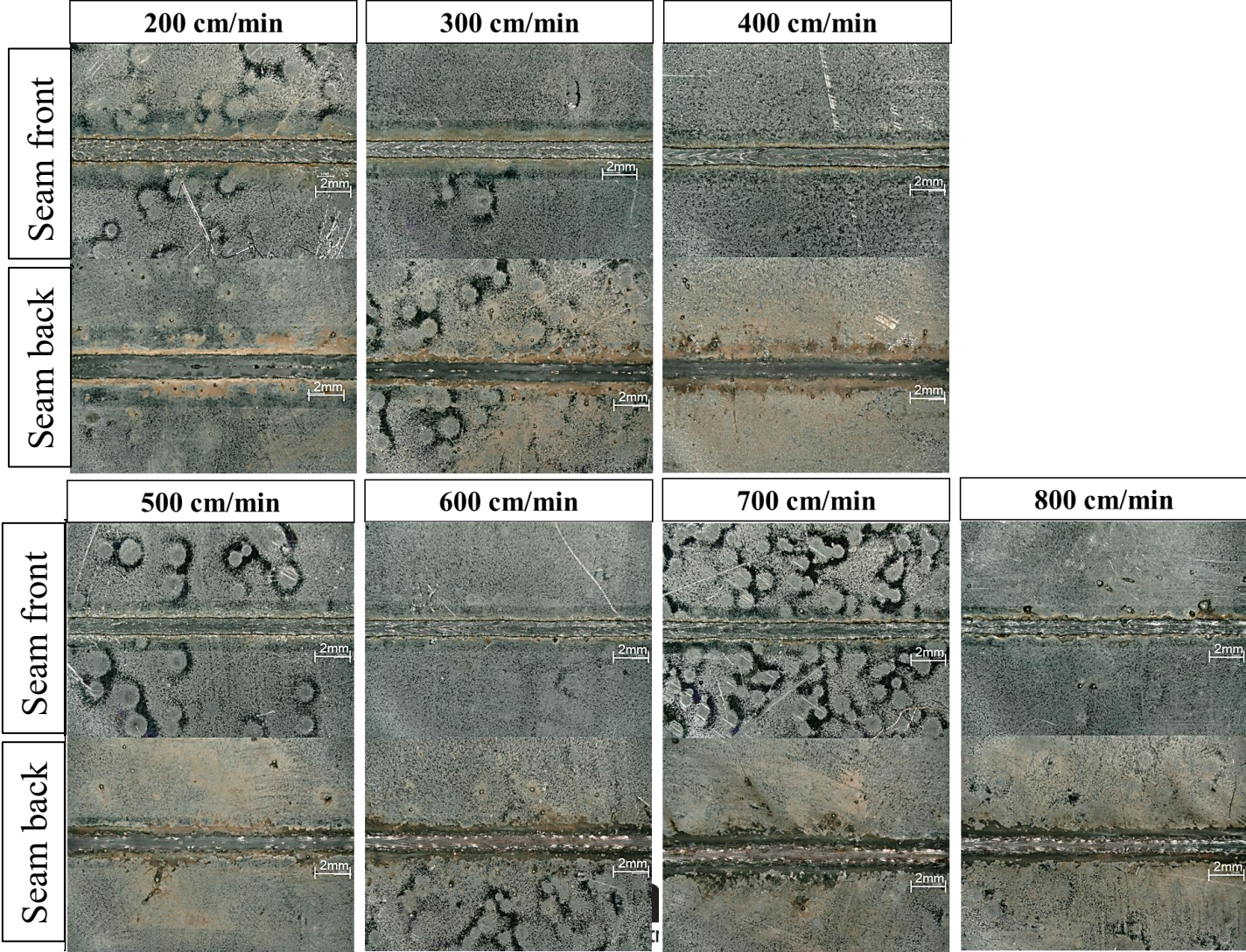
WELD PROPERTIES

Weld Appearance

T3 welds: 1.2 mm laser spot size



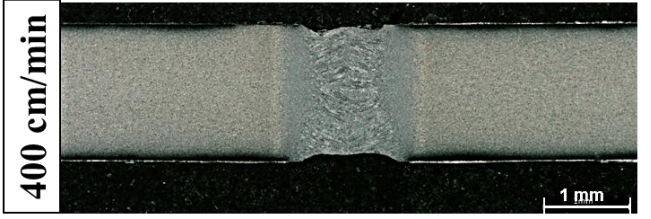
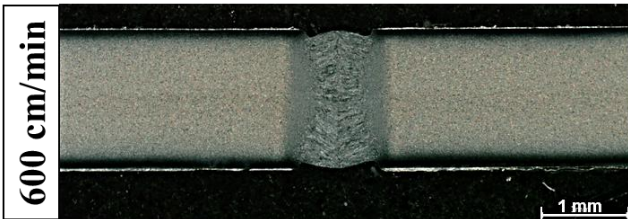
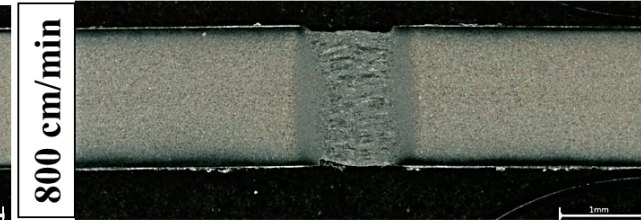
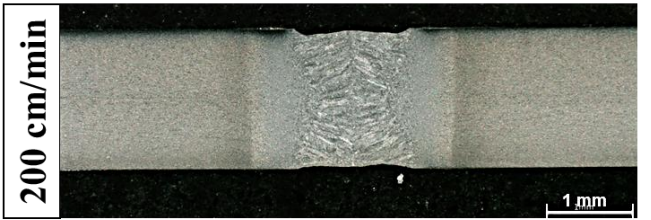
T1 welds: 0.3 mm laser spot size



Cross-Sections of Laser Welds

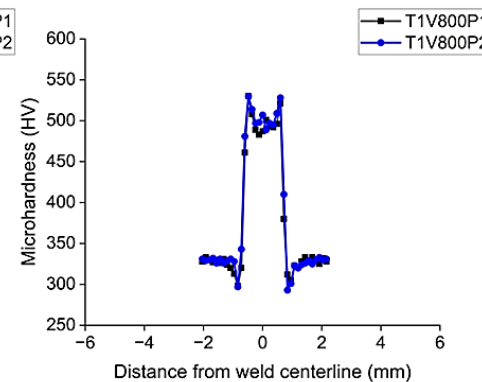
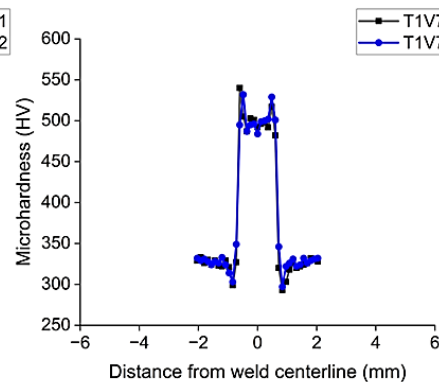
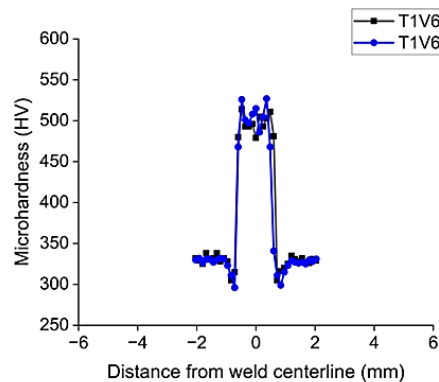
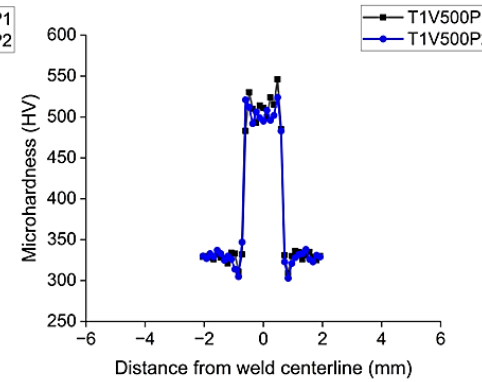
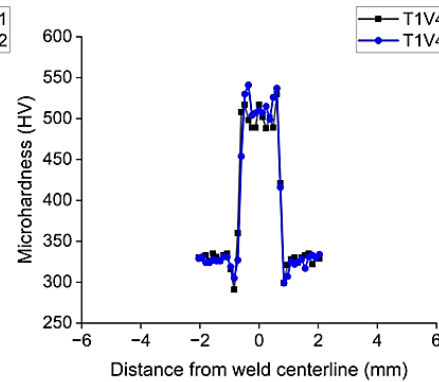
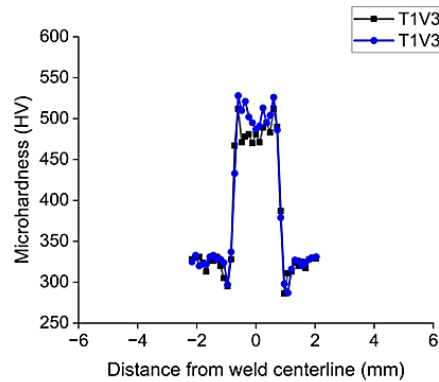
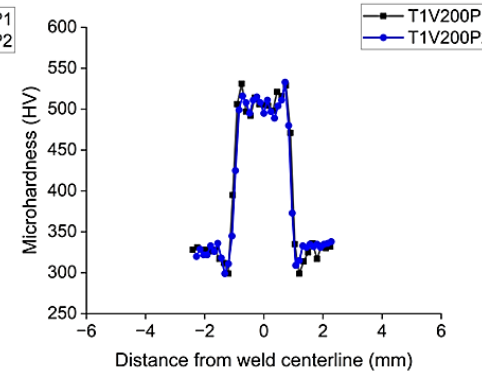
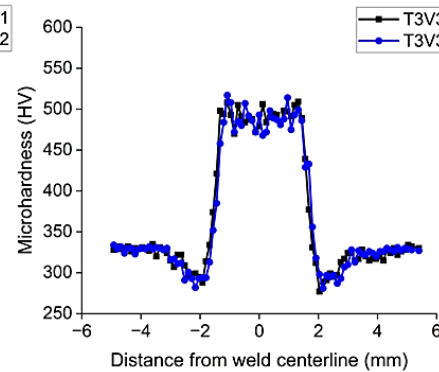
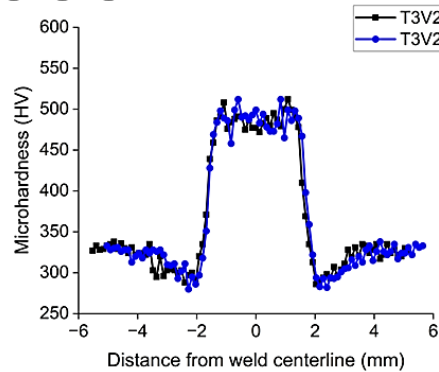


T3 Welds



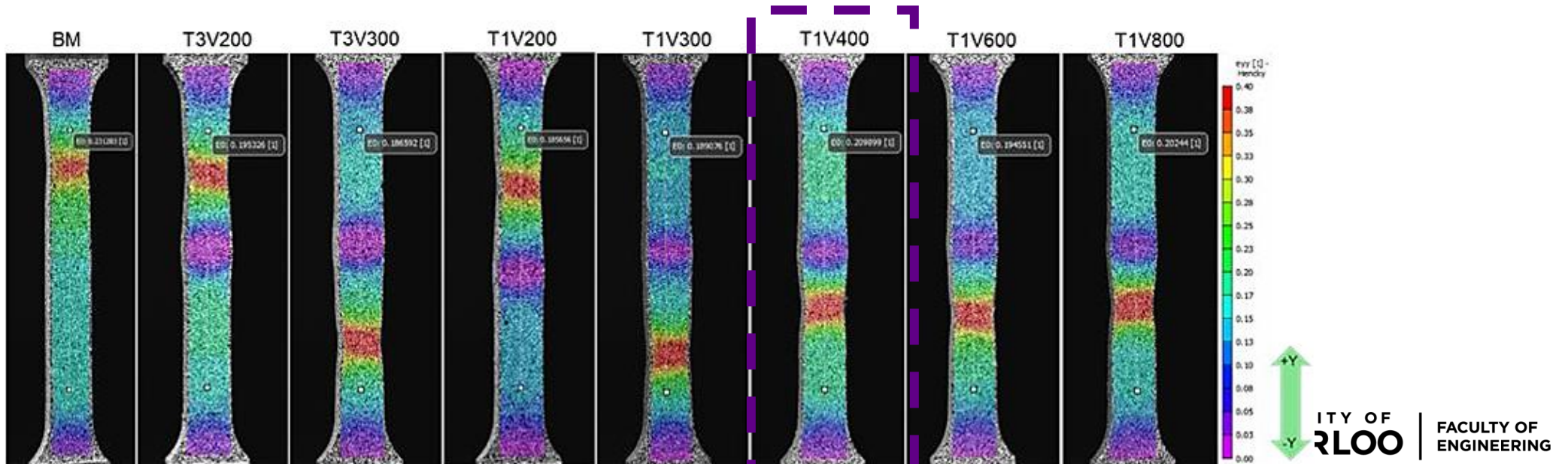
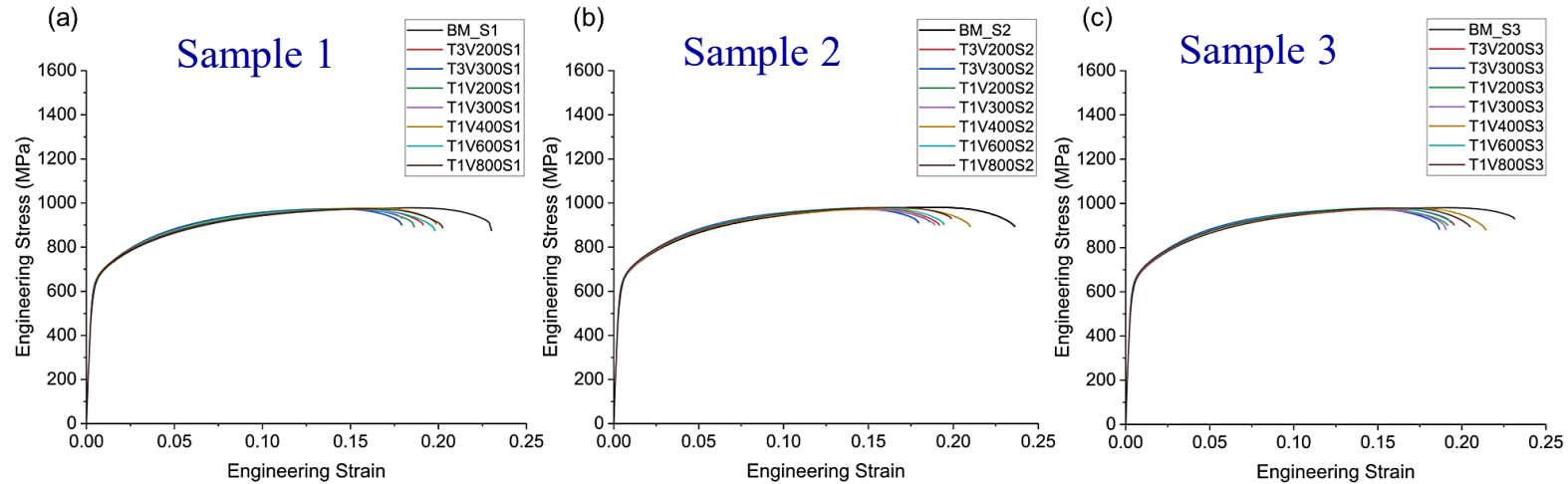
T1 Welds

Weld Hardness



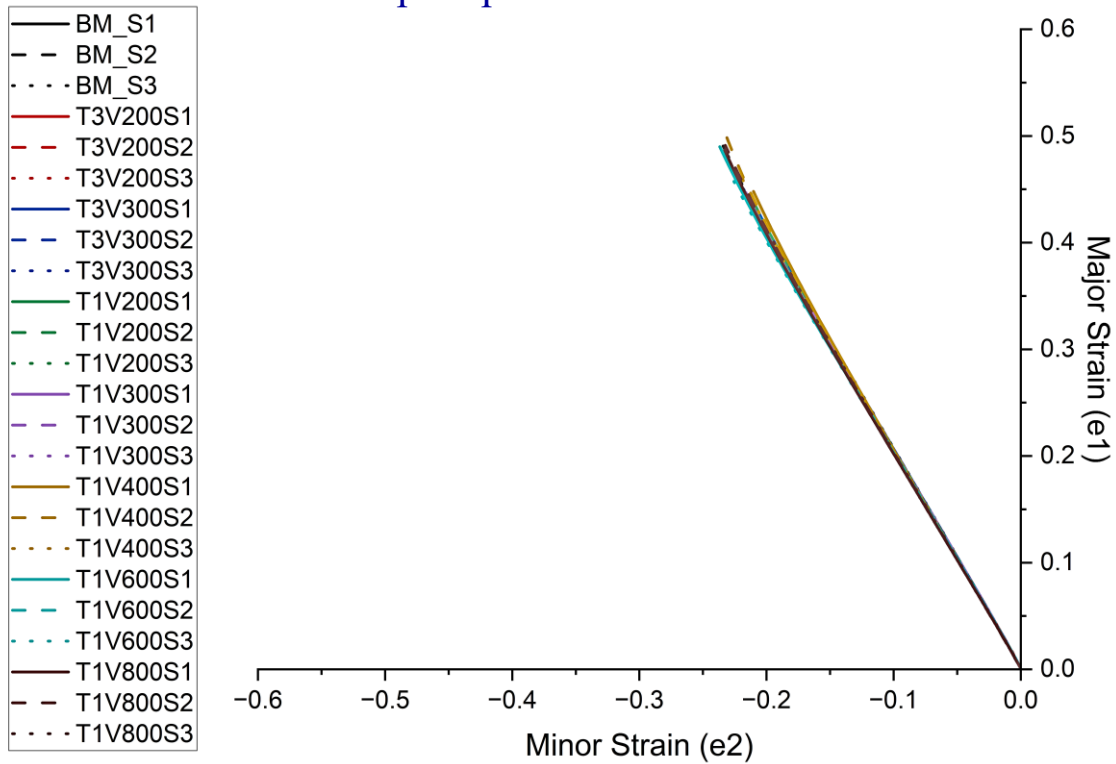
FORMING BEHAVIOUR

Tensile (Uniaxial Stretch) Behaviour of Welds

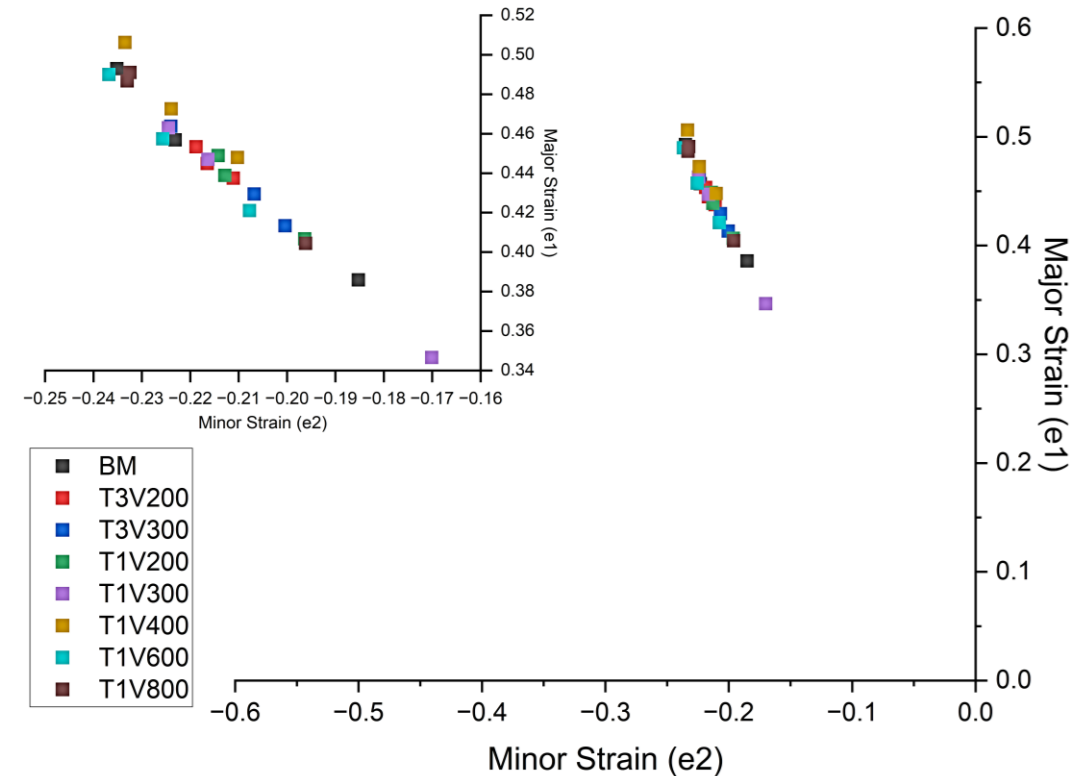


Strain Path of Welds Subjected to Tensile (Uniaxial) Strain

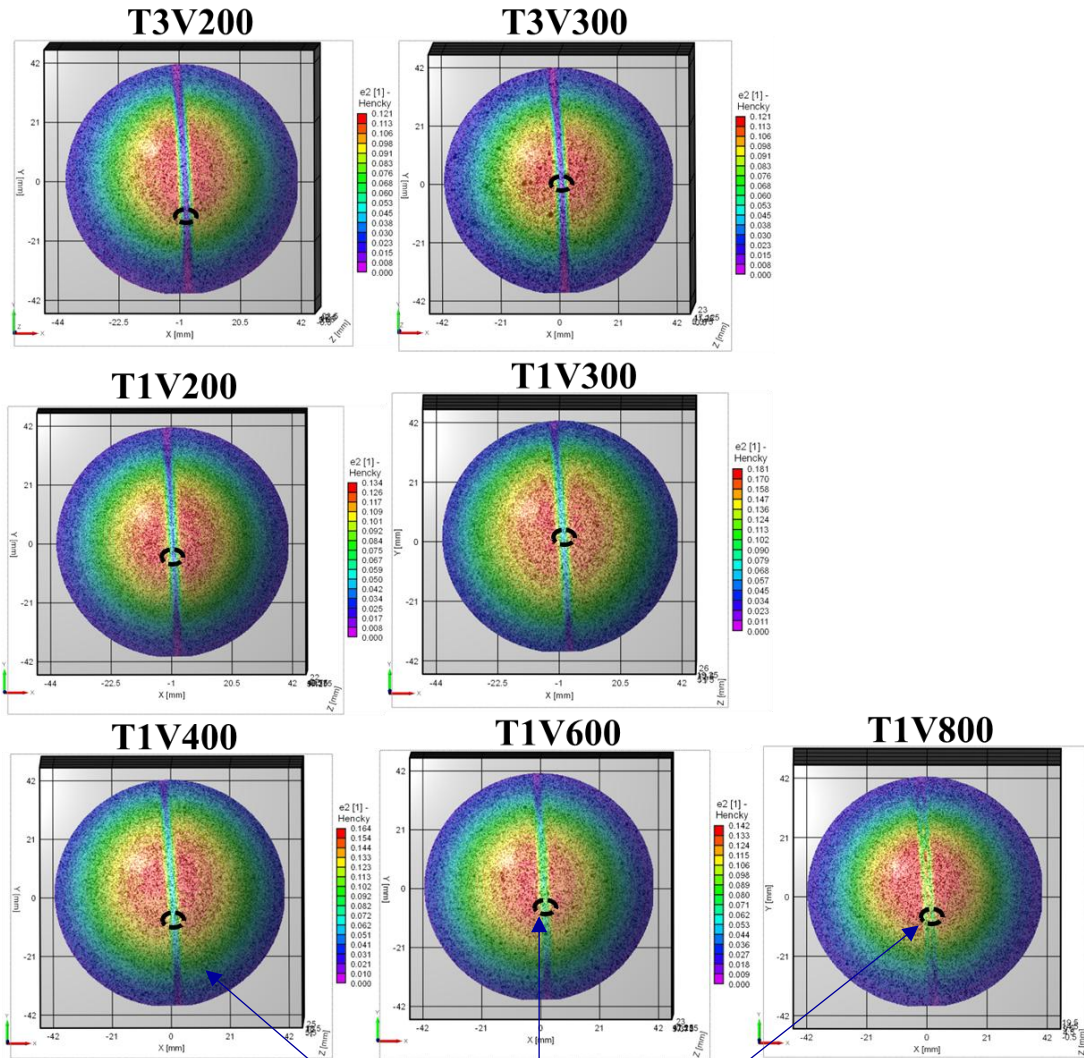
Strain path prior to fracture onset



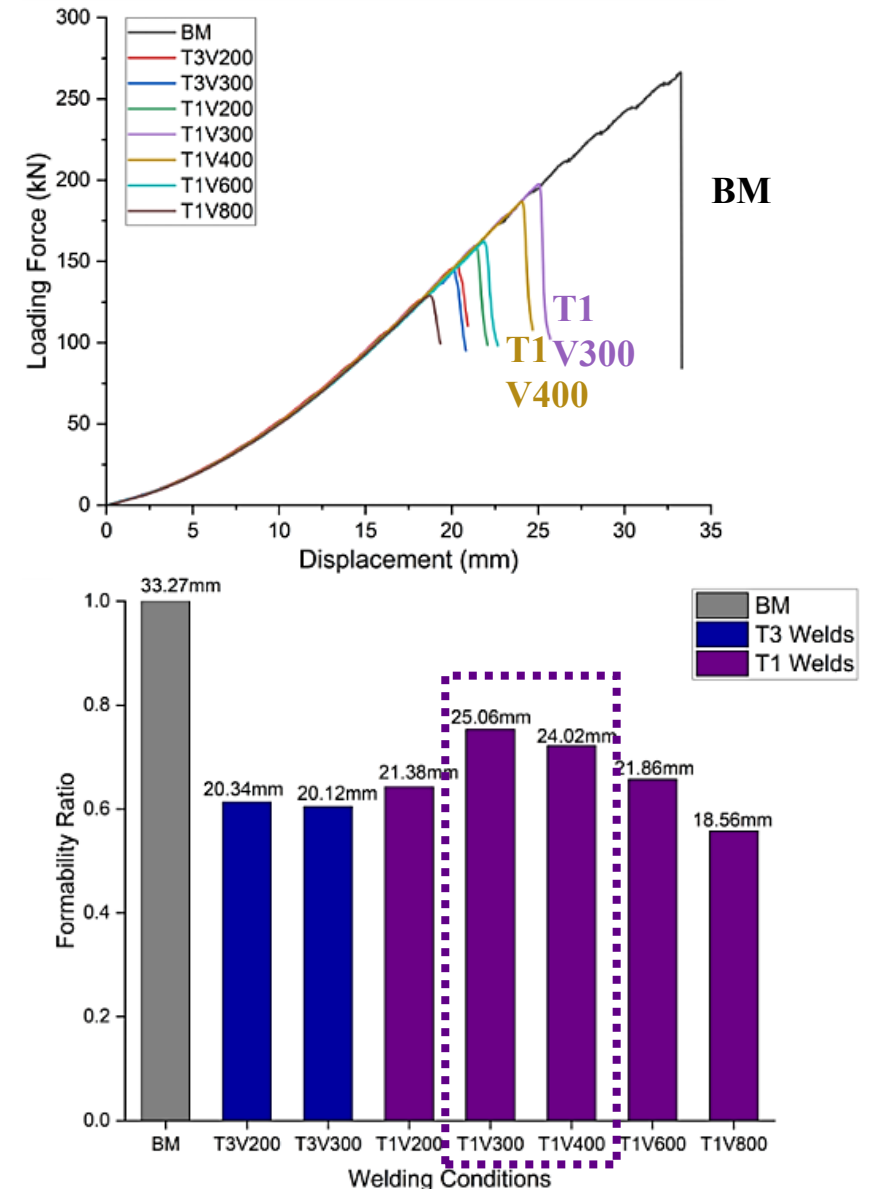
Strain values prior to fracture onset



Formability of TWB in Biaxial Stretch

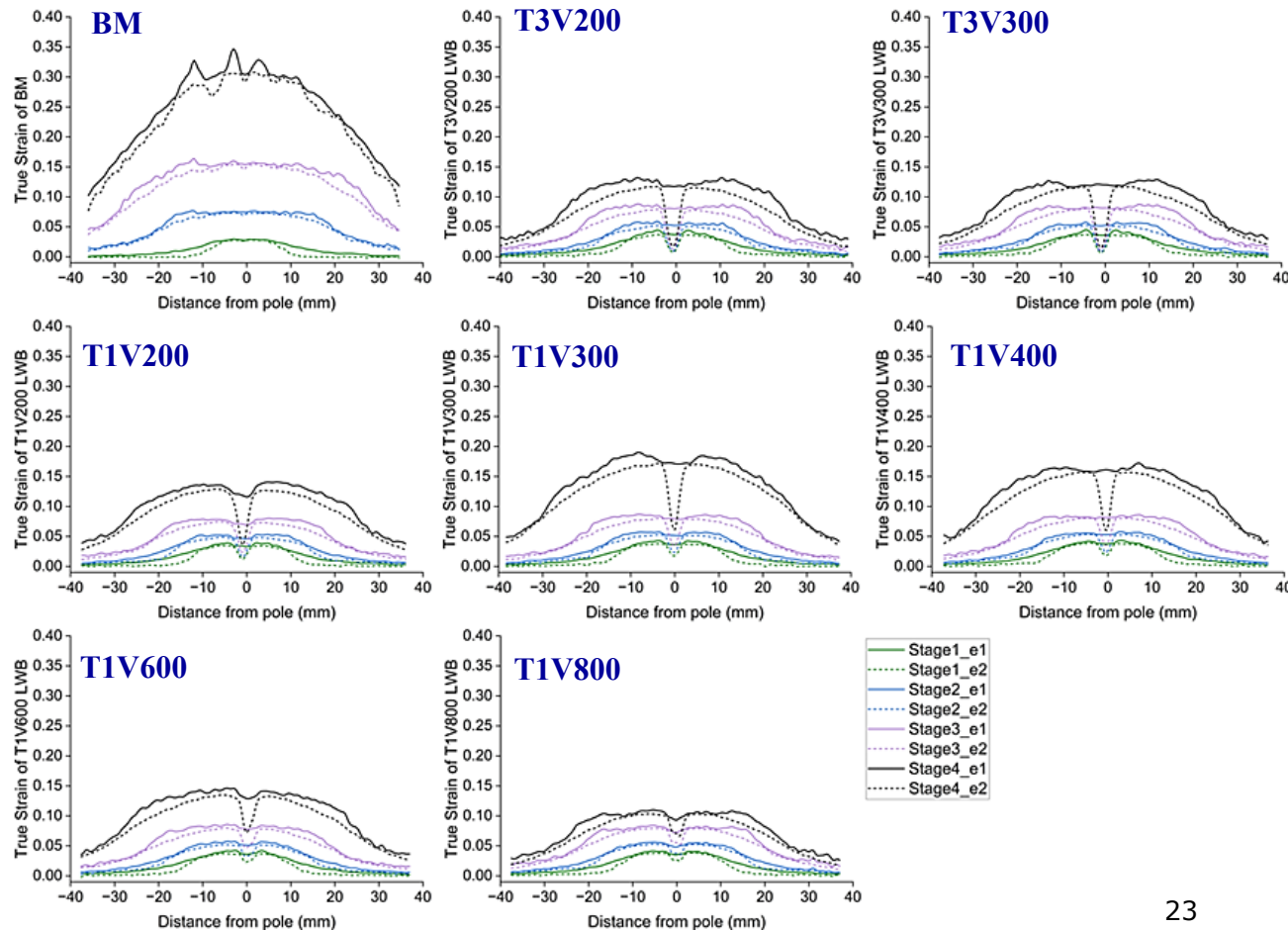


Fracture initiation location

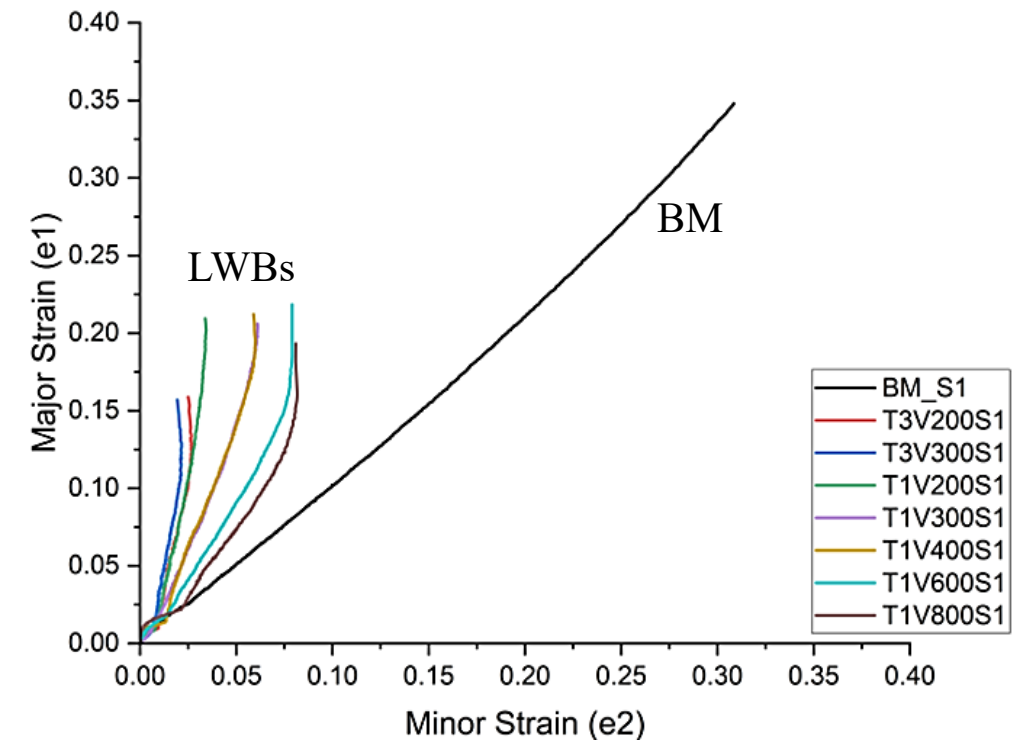


Strain Path During Biaxial Stretch

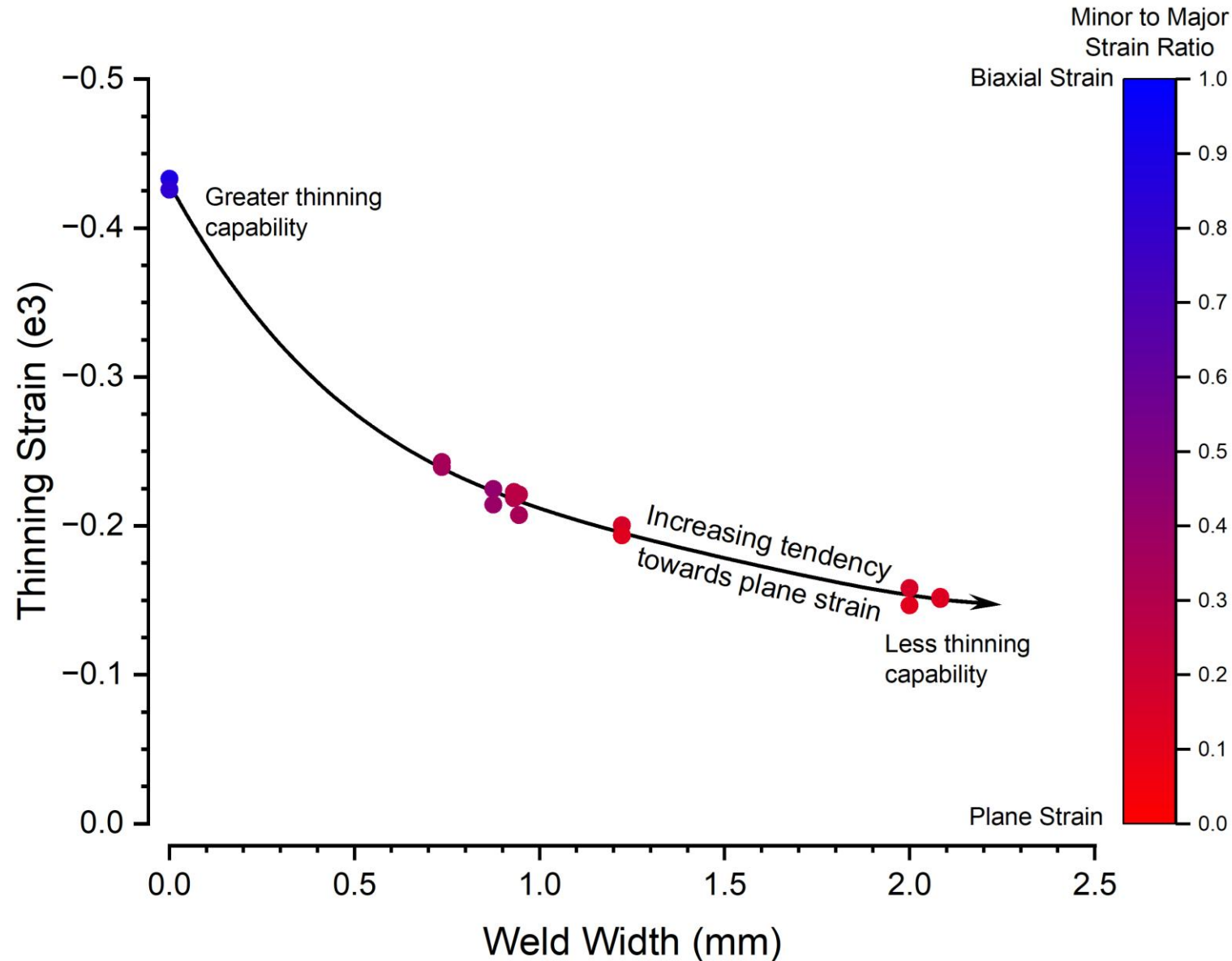
Local strain evolution along the pole and across the weld line over the entire deformation history



Strain path at fracture initiation site prior to cracking



Relation Between Weld Dimensions and Biaxial Formability



CONCLUSIONS

Conclusions

- Although welds loaded in tension (uniaxial stretch) perpendicular to the weld line showed some (22%) decrease in total elongation there was almost no decrease in joint strength (0.6% drop in UTS) and no change in strain path at the failure location compared to the monolithic blank
 - All samples failed in the base material
- The weld in the TWB changed both the maximum dome height, and strain patch of blanks in formed in biaxial stretch when compared to the monolithic blank.
 - The maximum dome height decreased between 25%-44% compared to the monolithic blank, and strain path approach to the plane strain condition from the biaxial strain conditions
- During biaxial testing all samples failed in the fusion zone
- Weld formability increased as fusion zone width decreased. However, at very narrow fusion zone widths, geometric defects limited blank elongation
- As fusion zone width decreased, the strain path at the failure location became more biaxial and higher thinning strains were achieved

Acknowledgements

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UNIVERSITY OF
WATERLOO



Thank you for your attention!

Elliot Biro – elliot.biro@uwaterloo.ca

Eric McCarty - emccarty@a-sp.org