

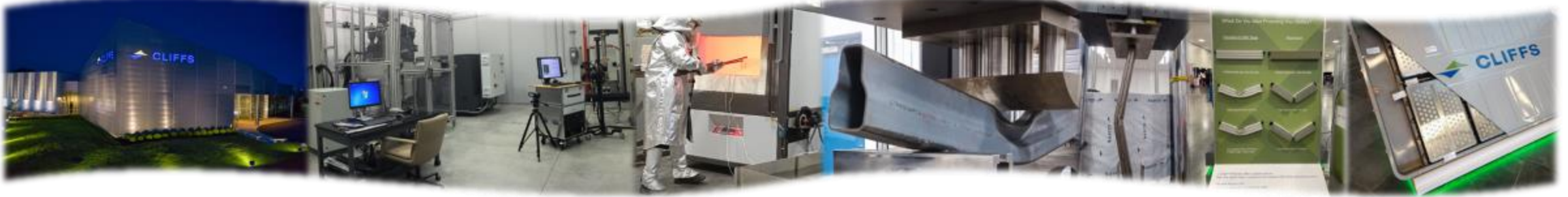
Comparative Study on Fracture Resistance of Ultra-High-Strength Press-Hardened Steels (UHS-PHSs)

Jun Hu, PhD
Cleveland-Cliffs Inc.



GREAT DESIGNS IN
STEEL™

Acknowledgements



The presenter extends sincere gratitude to Eliseo Hernandez-Duran (co-author), Chris Copeland, Steven Walls, Matt Faulkner, Chris Walker, Jason Wymer, Koushik Balasubramanian, Laura Burroughs, Grant Thomas, Dana Lentz, and numerous colleagues for their efforts and discussions in this and previous studies. The support from Cleveland-Cliffs Inc. management is also deeply appreciated.

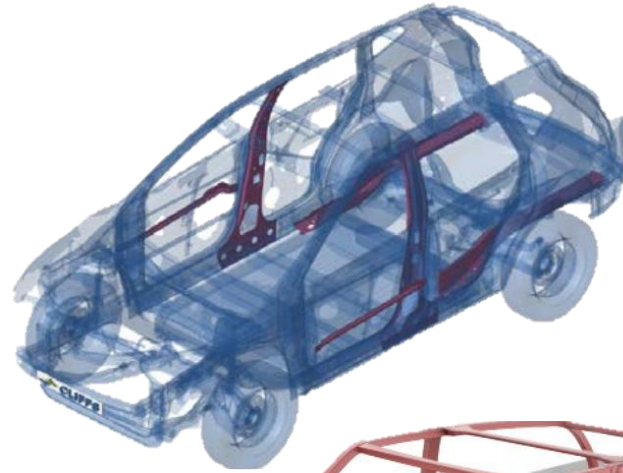
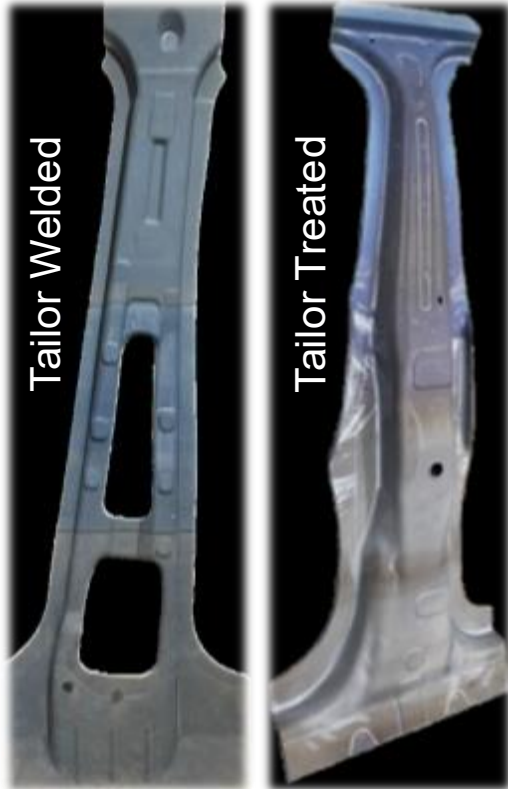


CLIFFS Offers PH(Q)S500|1000*|1500|2000*

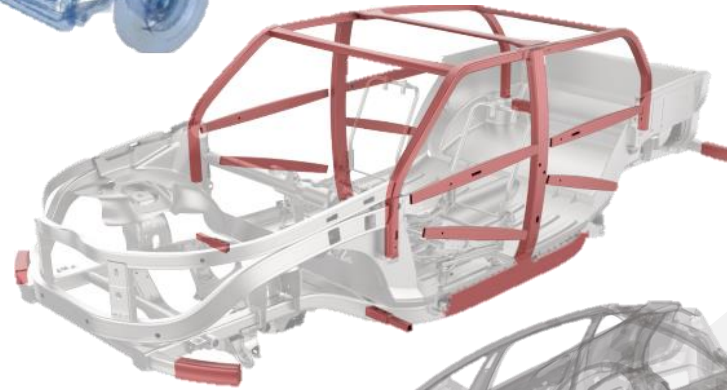
GDIS

*In development

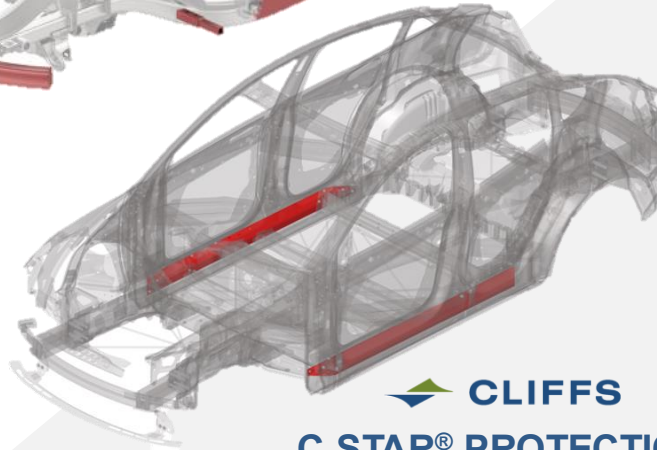
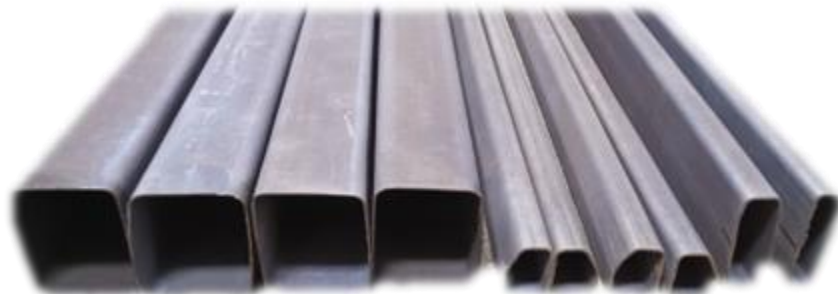
3



CLIFFS
ULTRALUME® PHS



CLIFFS
FORMTUBE® QHS



CLIFFS
C-STAR® PROTECTION

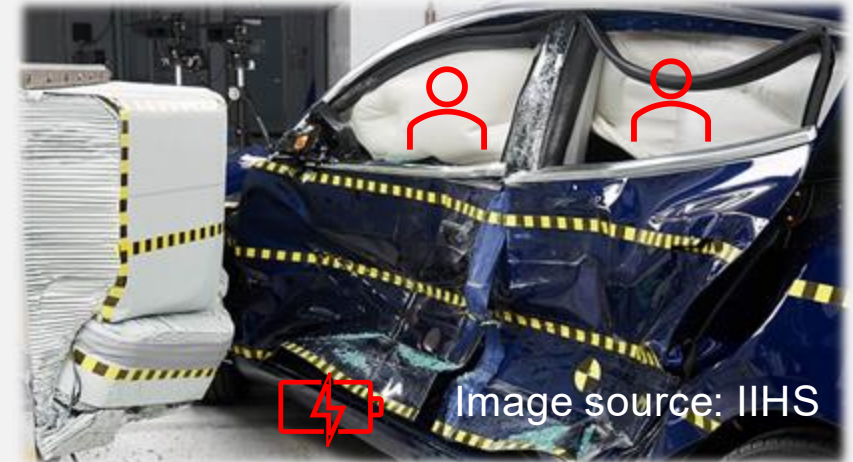


Image source: IIHS

More PH(Q)S Studies in Past GDIS

GDIS

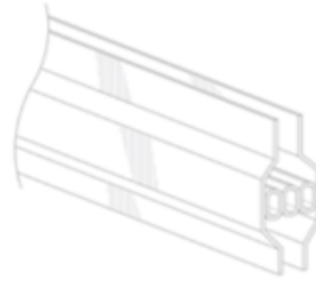
4

GREAT DESIGNS IN STEEL

2023

NEW STEEL TUBE DESIGN FOR BEV BATTERY
ENCLOSURE PROTECTION –
C-STAR™ (CLIFFS STEEL TUBE AS
REINFORCEMENT)

Miao Yu
Cleveland-Cliffs Inc.
Advanced Applications Engineer

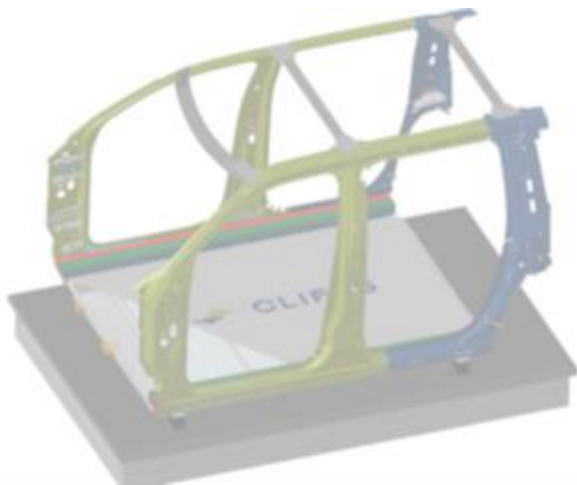


GREAT DESIGNS IN STEEL

2024

ULTRALUME® STEELS FOR HOT
STAMPING OF AUTOMOTIVE
STRUCTURAL COMPONENTS

Dr. Eliseo Hernandez-Duran
Cleveland-Cliffs Inc.
Product Research Engineer



GREAT DESIGNS IN STEEL

2024

Discrepant Paint-Baking Impact on
AHSSs and HSAAs Used in BEV
Structures

Jun Hu, PhD
Cleveland-Cliffs Inc.

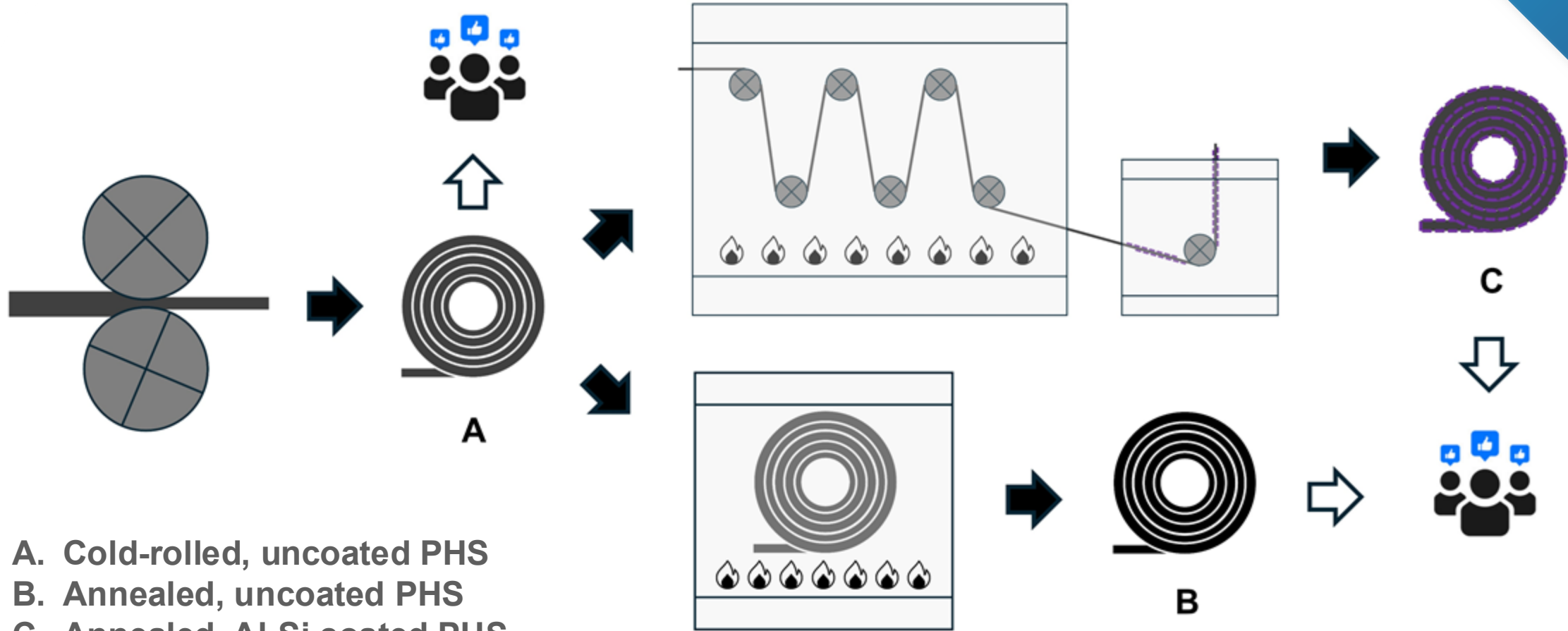


CLIFFS Offers 3 Types of PHS1500|2000*

*In development

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- A. Cold-rolled, uncoated PHS
- B. Annealed, uncoated PHS
- C. Annealed, Al-Si coated PHS
(most demanded type)

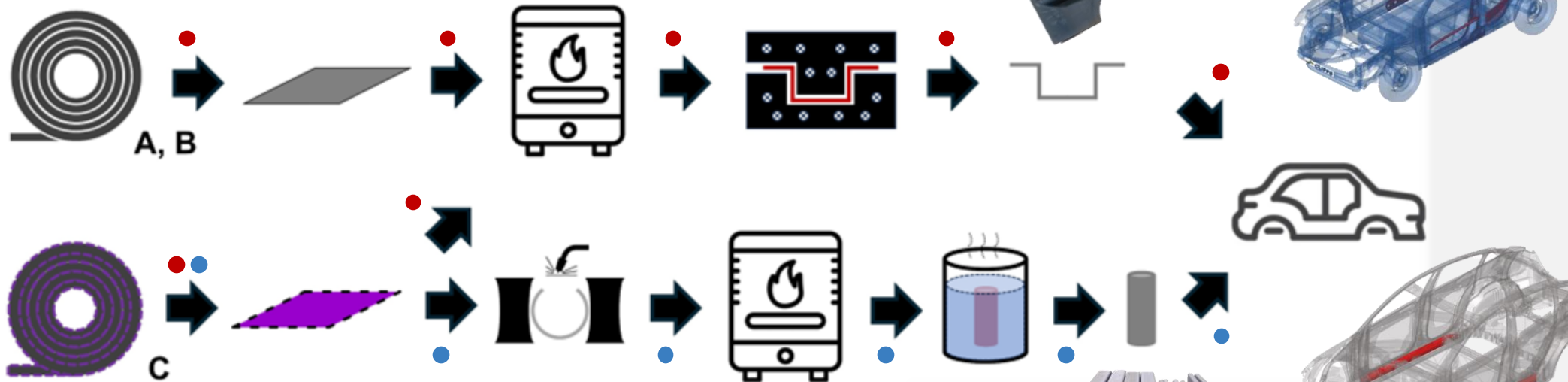
3 Types of PHS1500|2000 in Forming

GDIS

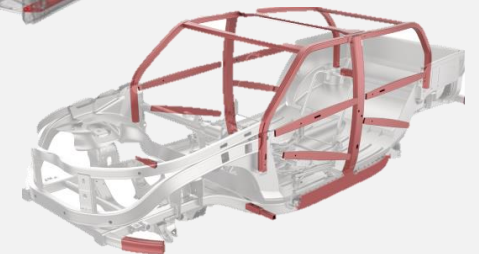
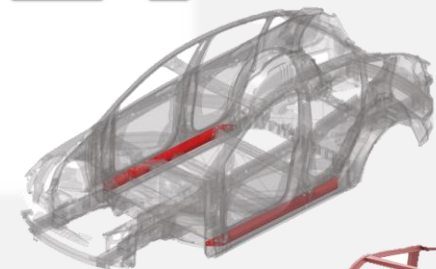
6



Hot-Stamped → Die-Quenched



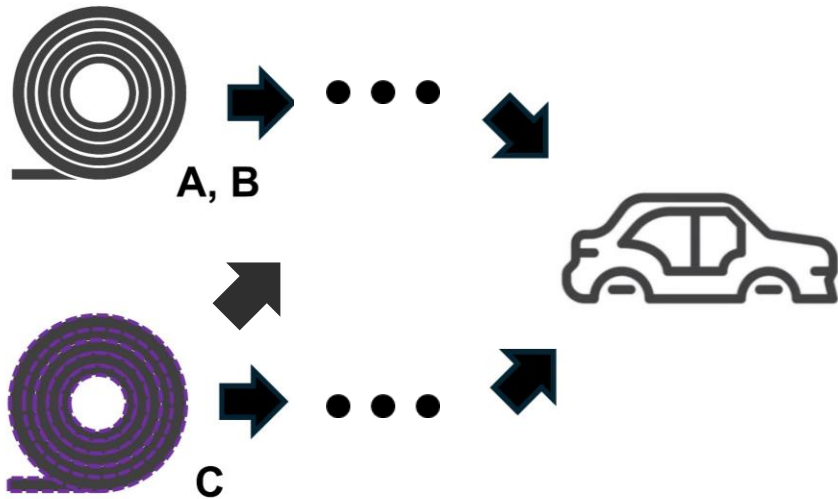
Cold-Rolled → Annealed → Liquid-Quenched



3 Types of PHS1500|2000 in Paint-Baking

- A. Cold-rolled, uncoated PHS
- B. Annealed, uncoated PHS
- C. Annealed, Al-Si coated PHS

**Hot-Stamped → Die-Quenched
→ Paint-Baked**



**Cold-Rolled → Annealed →
Liquid-Quenched → Paint-Baked**

Microstructure evolution: ferritic → austenitic
→ fresh martensitic → tempered martensitic

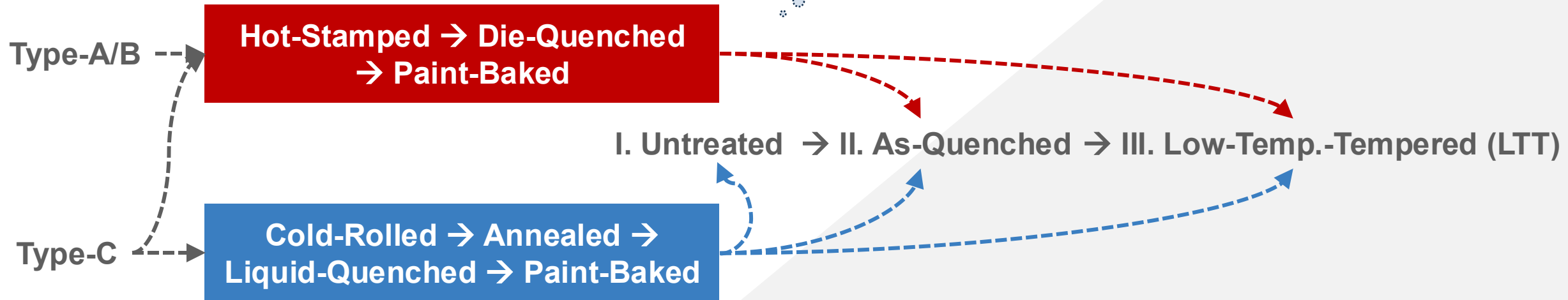


Paint-baking = low-temperature-tempering (LTT) can lower the micro-hardness of fresh martensite and eventually improve the fracture resistance of PHS1500|2000-AS (Type-C in this work) (CHS² 2024 and GDIS 2024)

3 Critical Stages & Research Motivation

- A. Cold-rolled, uncoated PHS
- B. Annealed, uncoated PHS
- C. Annealed, Al-Si coated PHS

How does the fracture resistance evolve in the 3 stages?



Fracture resistance / fracture strain / local ductility ≠ global ductility / tensile elongation
(SAE 2022, GDIS 2023, AIST Trans. 2024)

Evolving Fracture Resistance of PHS1500|2000

GDIS

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**From Untreated to
Quenched**



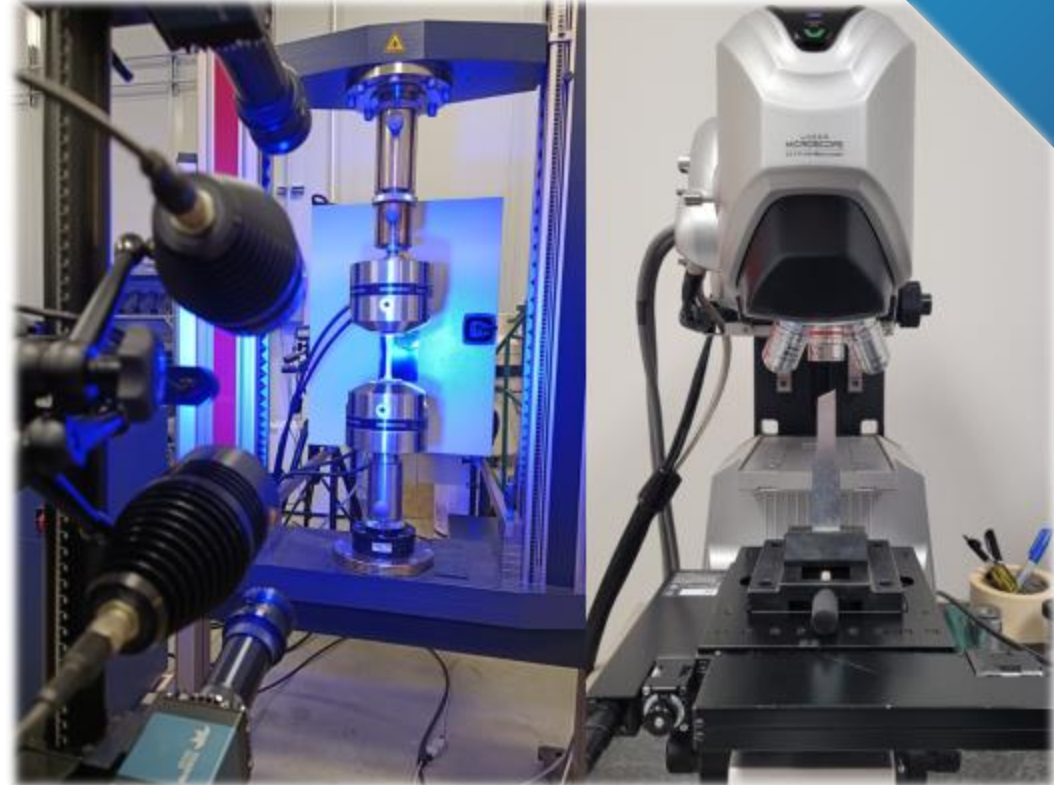
LTT (Paint-Baking) Effects



**Rate / Stress-State Effects
(on Type-A)**



Tensile Testing Procedure

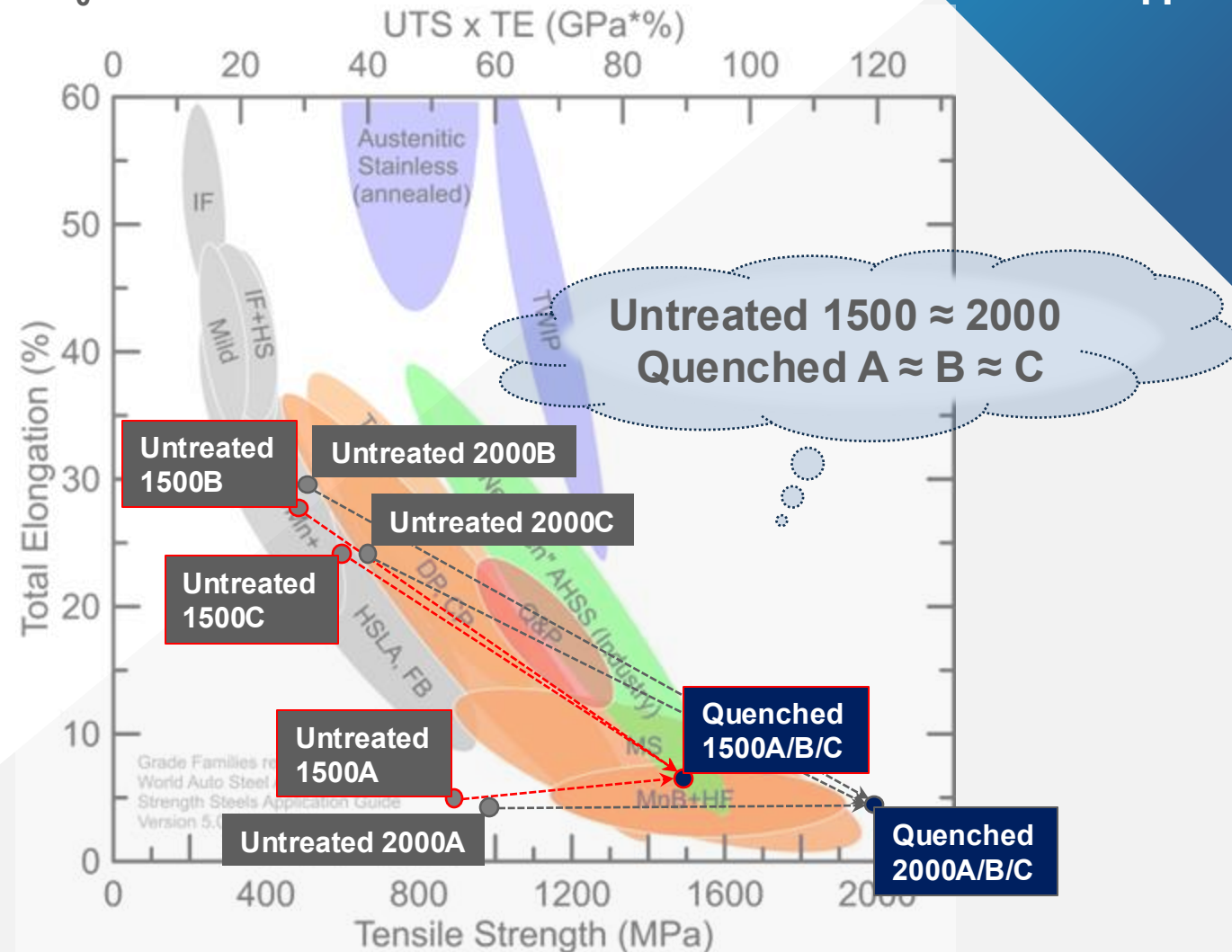
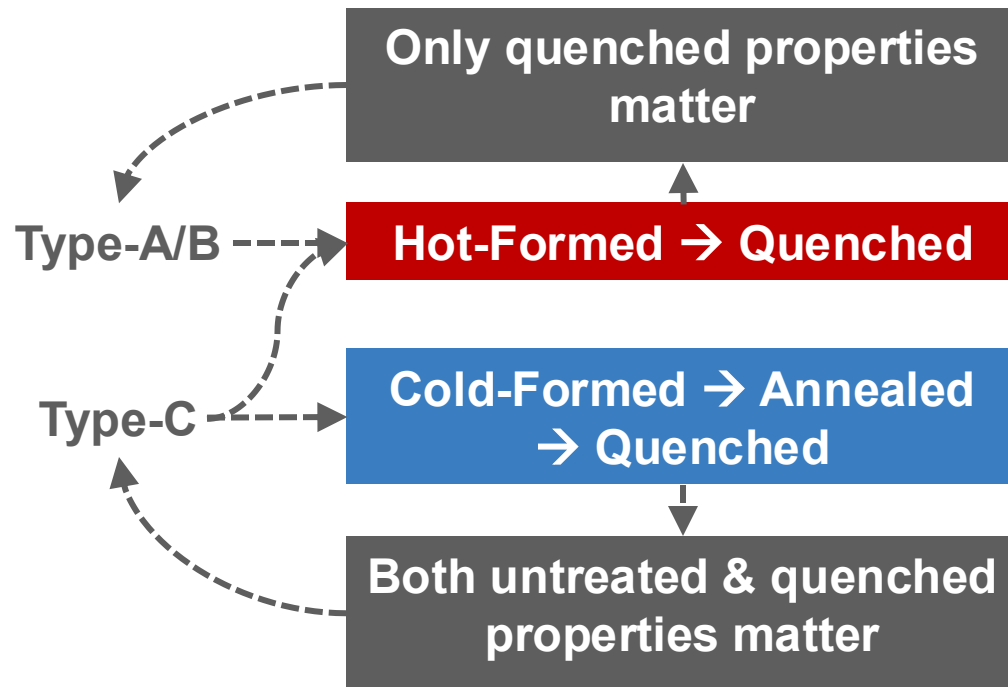


Hot-stamping: each blank was heat-treated in an oven at 930°C for 5 min. → fully die-quenched at 300°C/s

Fracture strain measurement based on the hybrid DIC-microscopic method (SAE 2022, GDIS 2023) of virtual strain gauge length (VSGL) 0.5 mm on longitudinal (L) ASTM E8 quasi-static tensile test samples

Results: Tensile Strength & Elongation

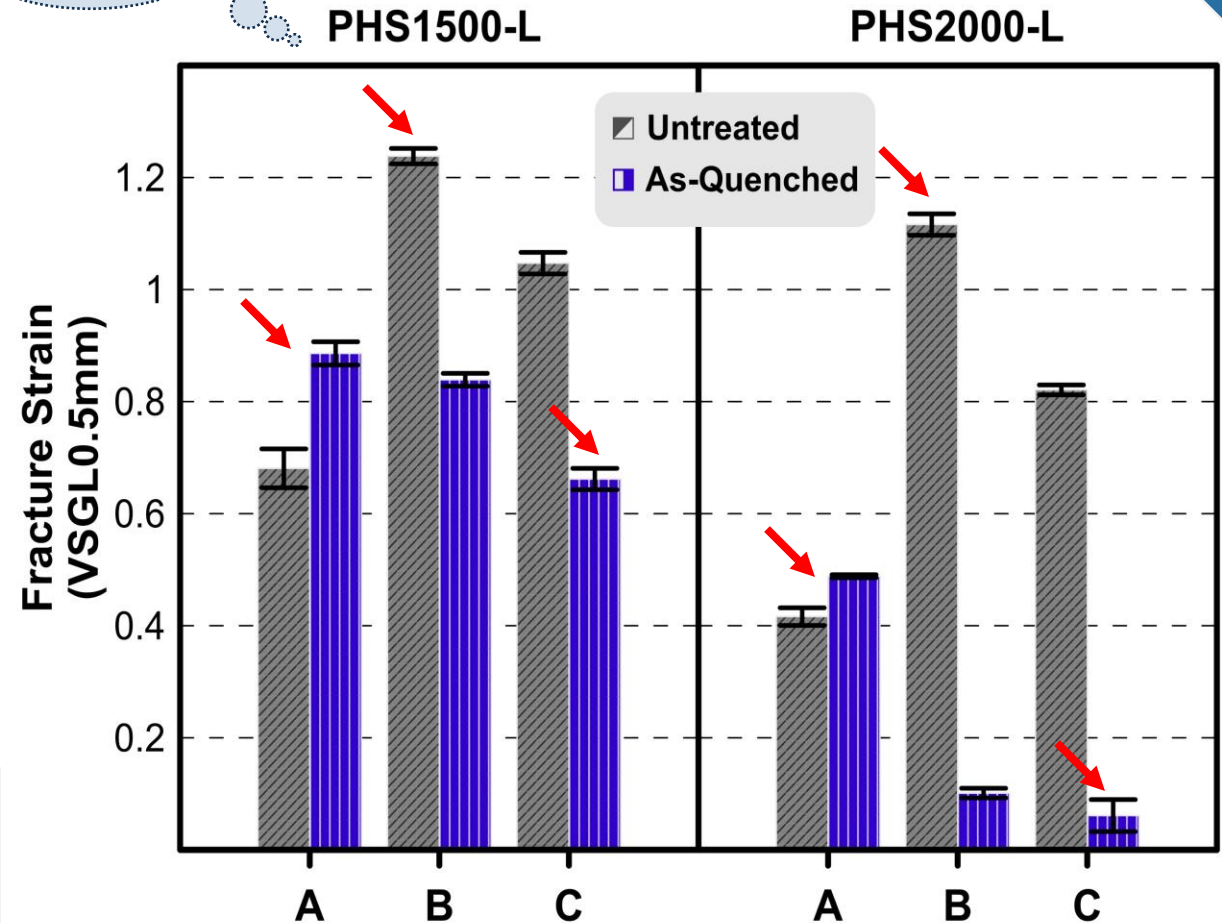
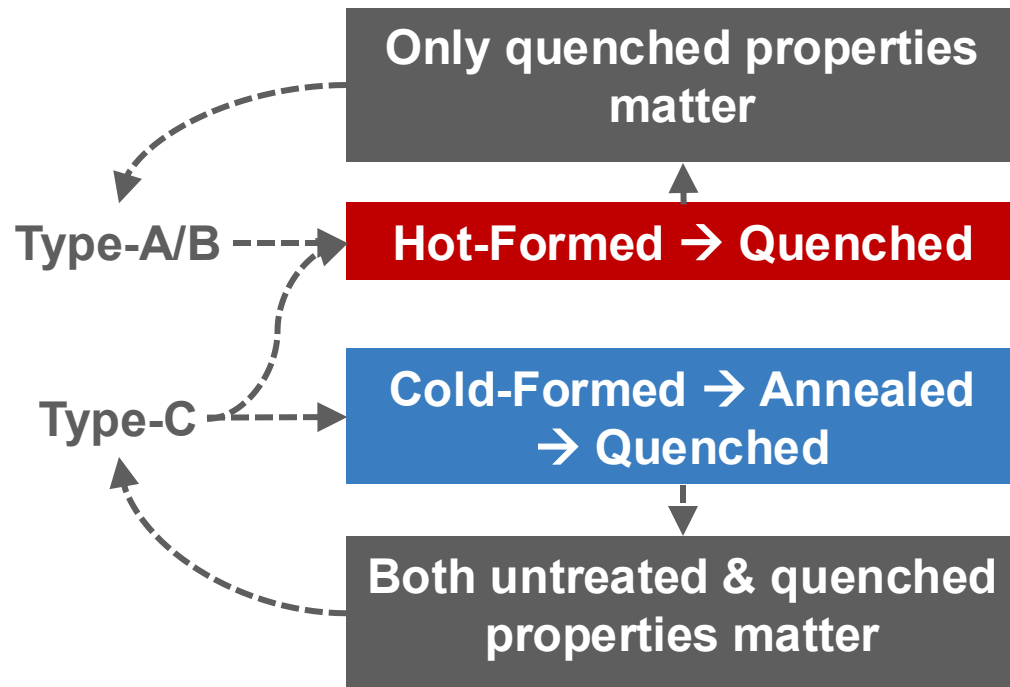
- A. Cold-rolled, uncoated PHS } Same nominal $t_0 = 1.8$ mm
B. Annealed, uncoated PHS }
C. Annealed, Al-Si coated PHS }



Results: Tensile Fracture Strain Fracture Strain ≠ Elongation

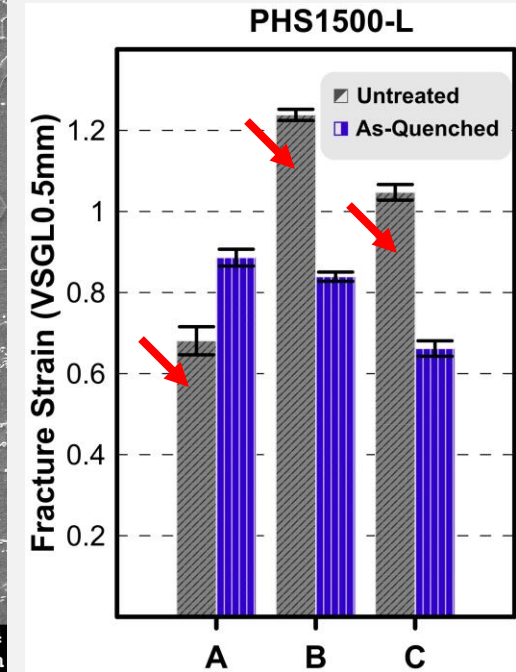
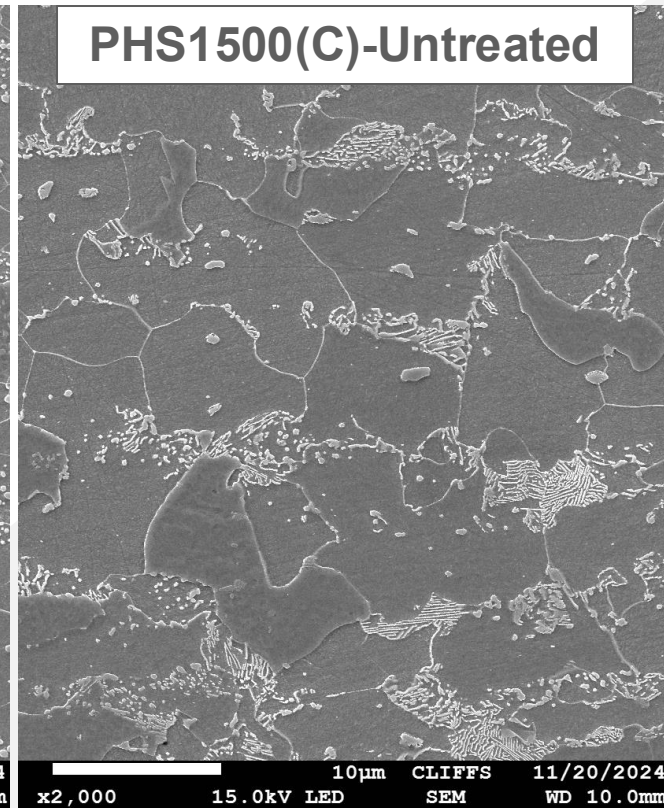
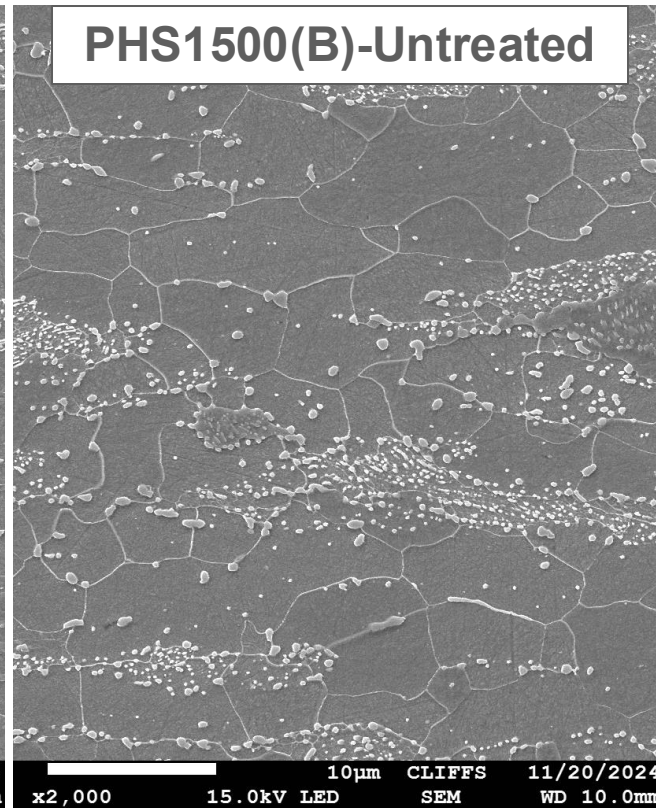
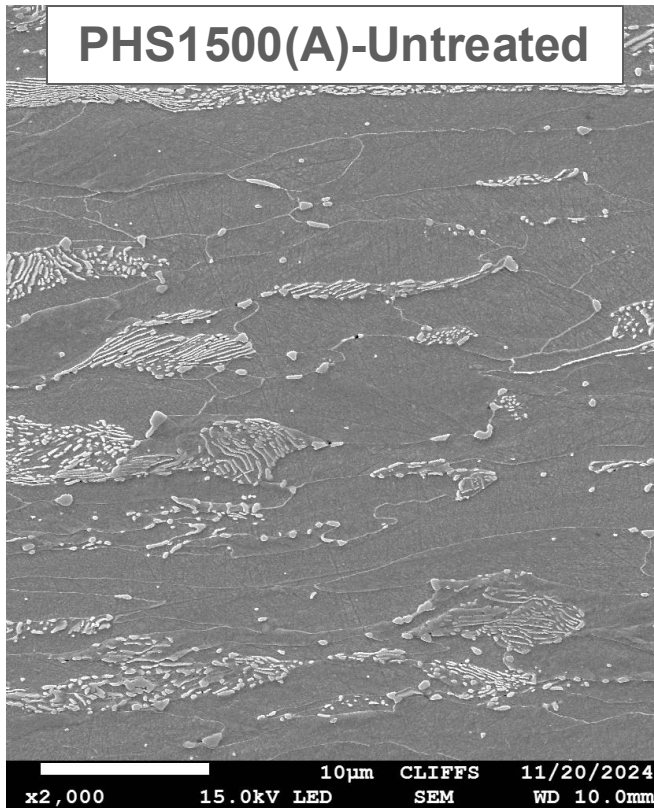
- A. Cold-rolled, uncoated PHS
- B. Annealed, uncoated PHS
- C. Annealed, Al-Si coated PHS

Annealing effects?
Coating effects?



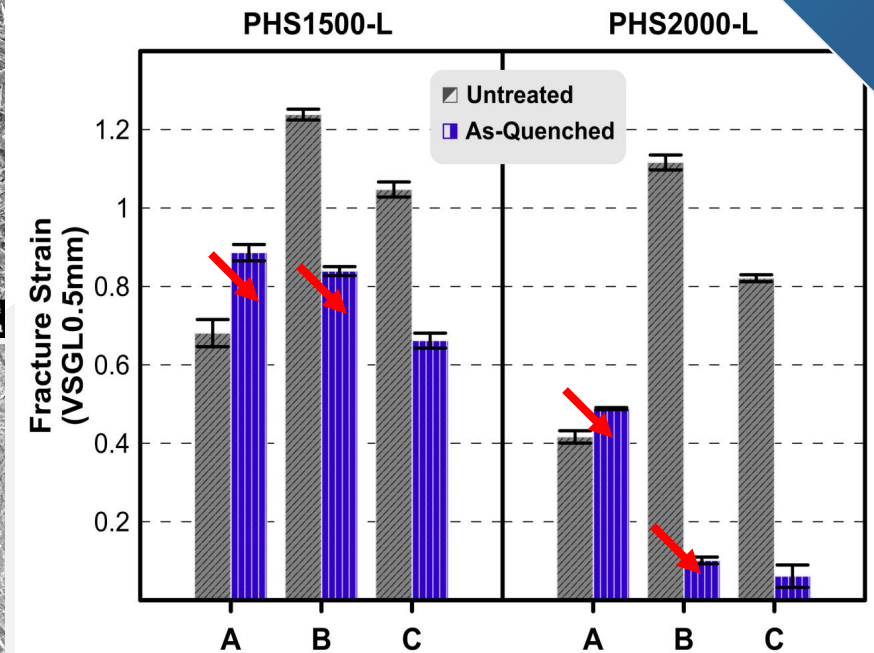
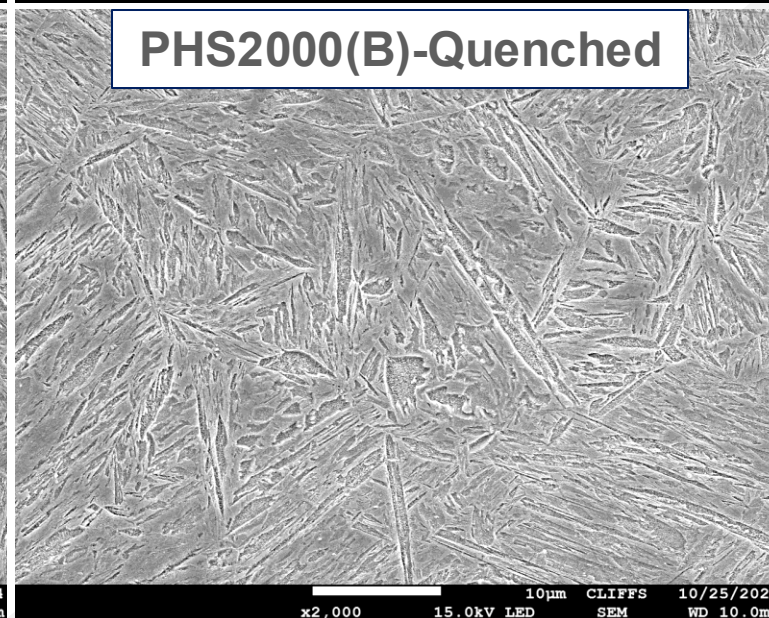
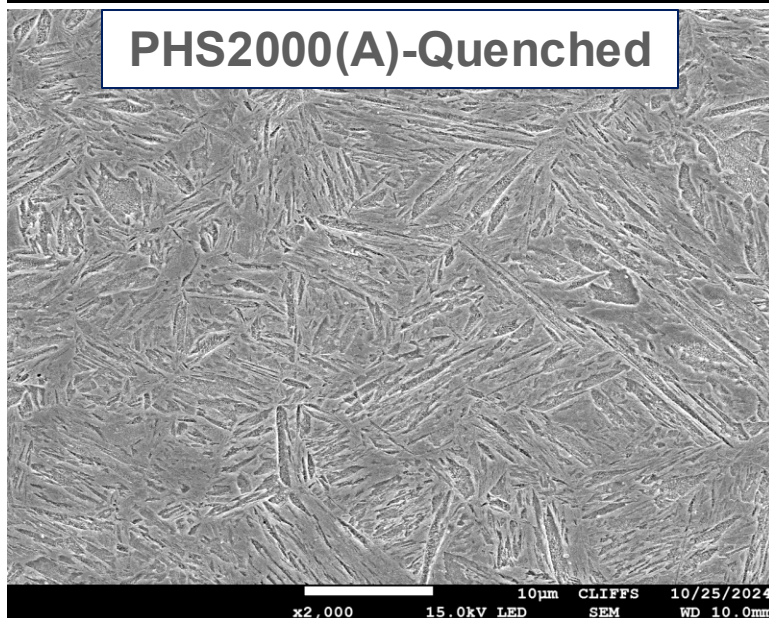
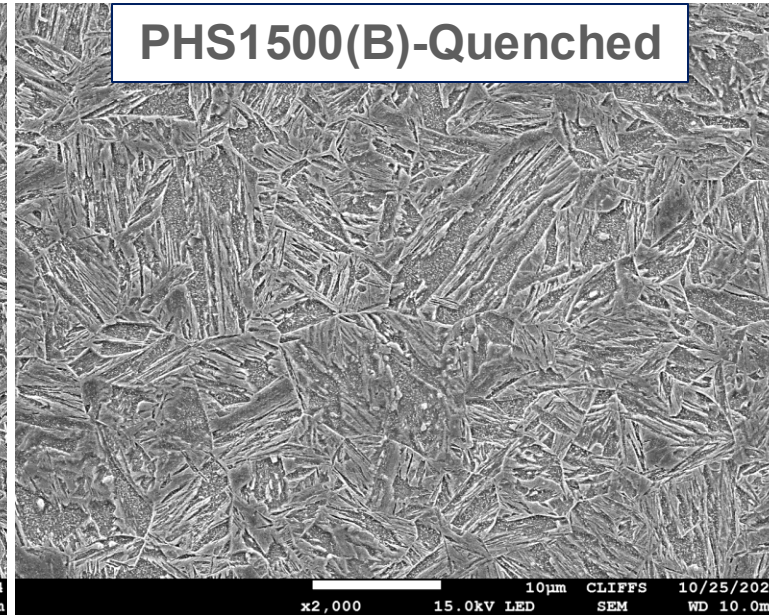
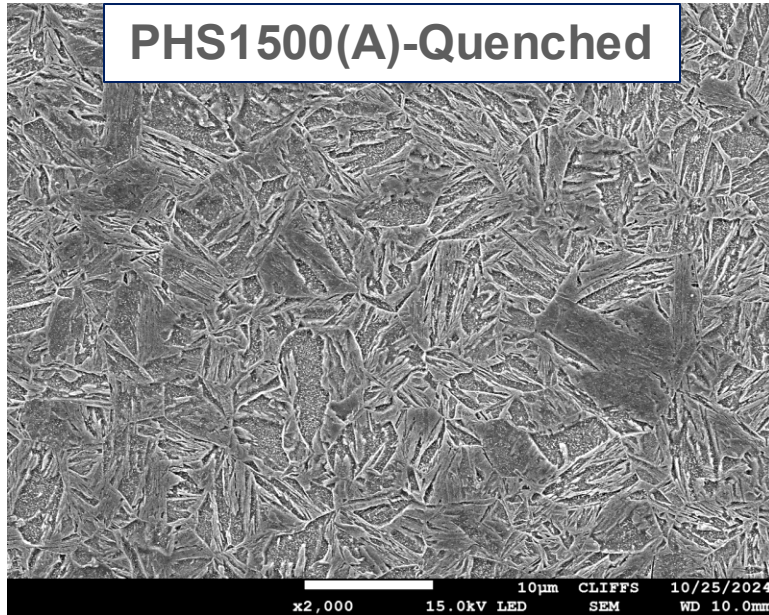
Annealing Effects on Untreated PHS1500

- A. Cold-rolled, uncoated PHS
- B. Annealed, uncoated PHS
- C. Annealed, Al-Si coated PHS



Annealing Effects on Quenched PHSs (A vs. B)

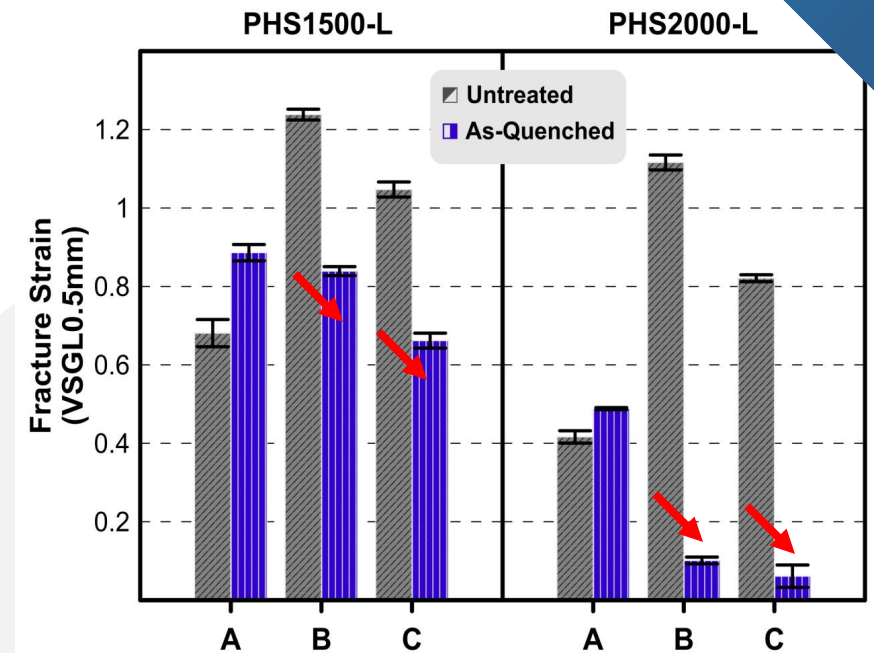
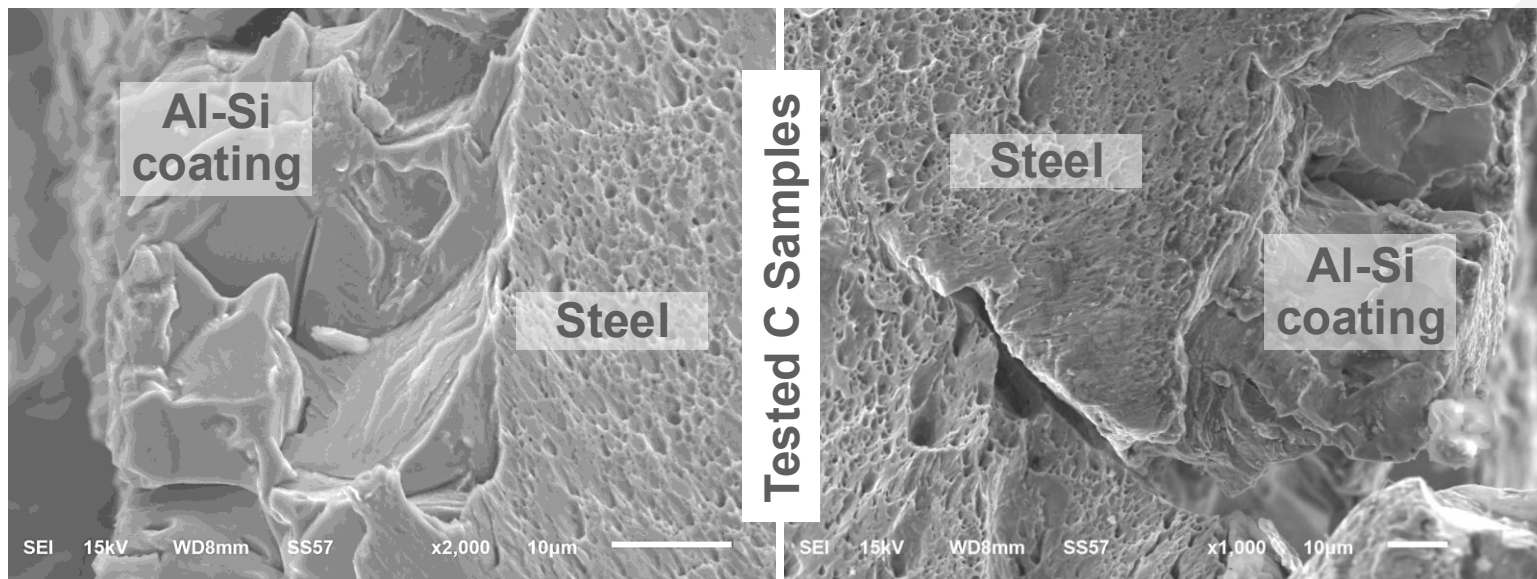
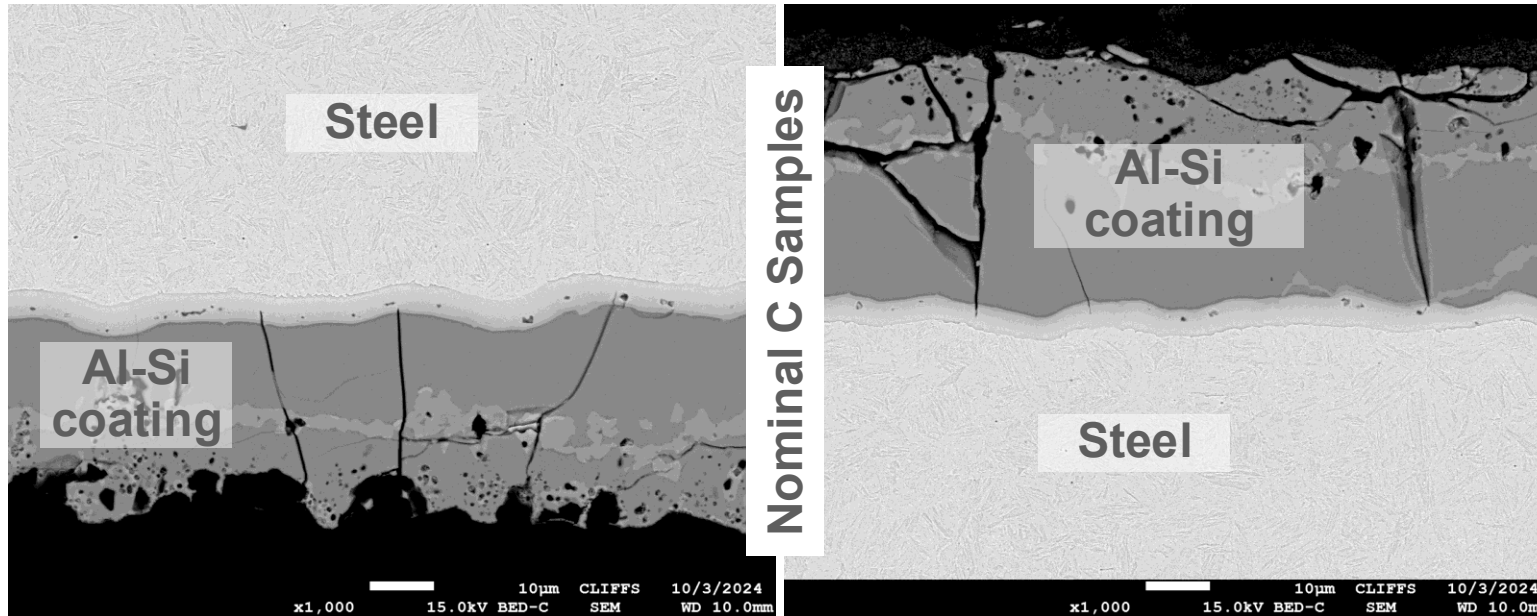
- A. Cold-rolled, uncoated
- B. Annealed, uncoated
- C. Annealed, Al-Si coated



Coarsened grains?

Coating Effects on Quenched PHSs (C vs. B)

- A. Cold-rolled, uncoated
- B. Annealed, uncoated
- C. Annealed, Al-Si coated



Pre-cracks from Al-Si coating

Summary of Tensile Ductility of 3 Types

A. Cold-rolled, uncoated

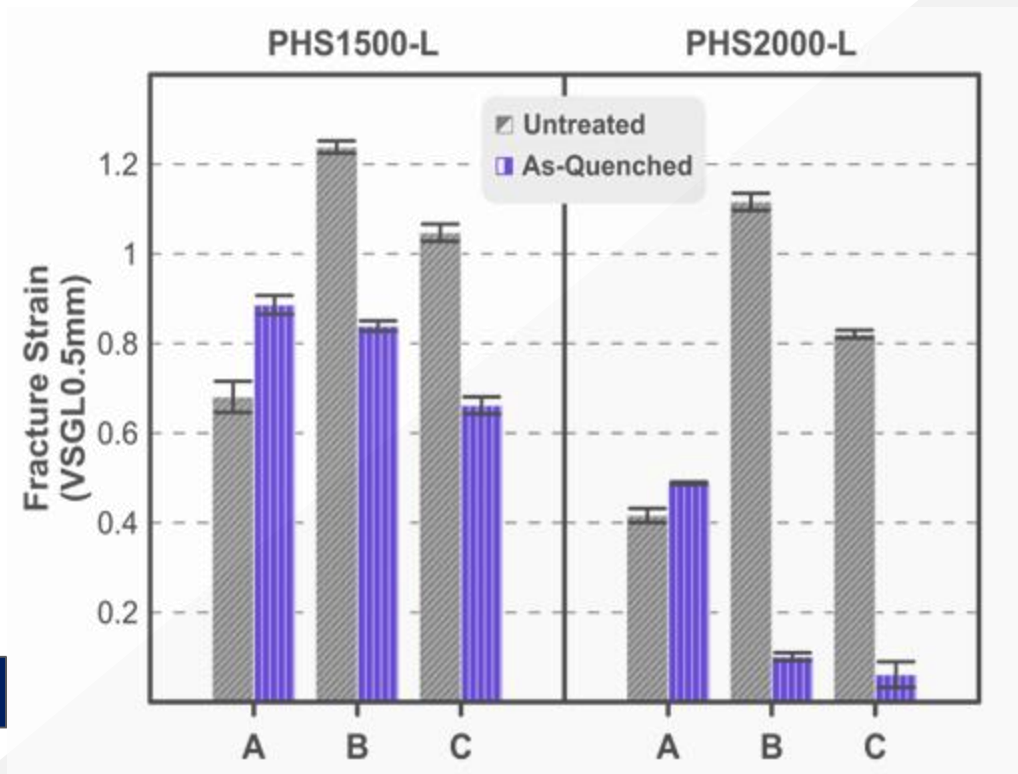
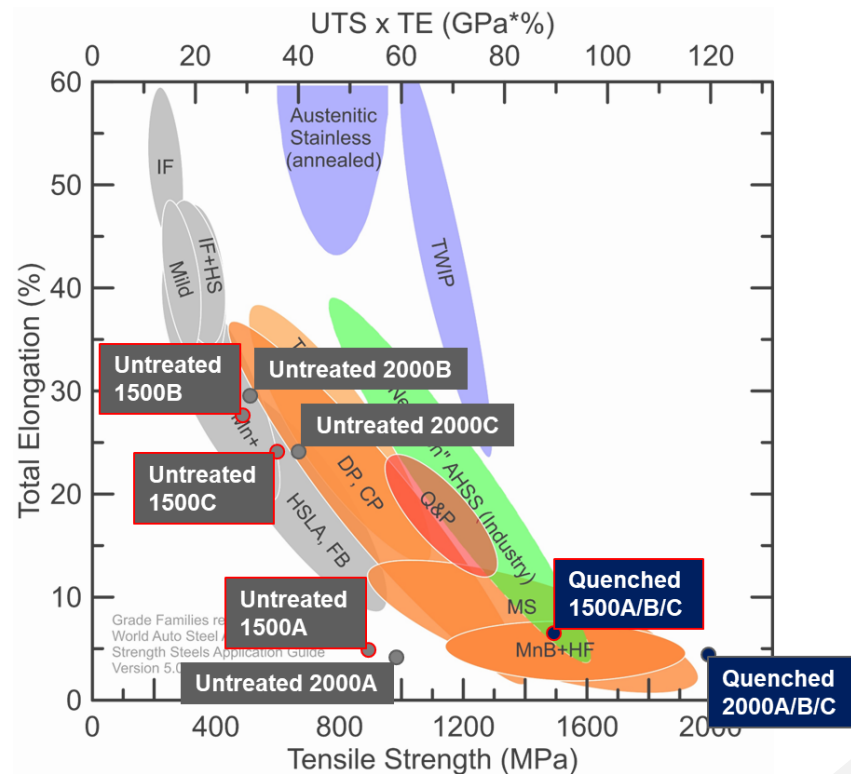
- Most brittle when untreated
- Most ductile after quenched
- Fracture strain increased after quenched

B. Annealed, uncoated

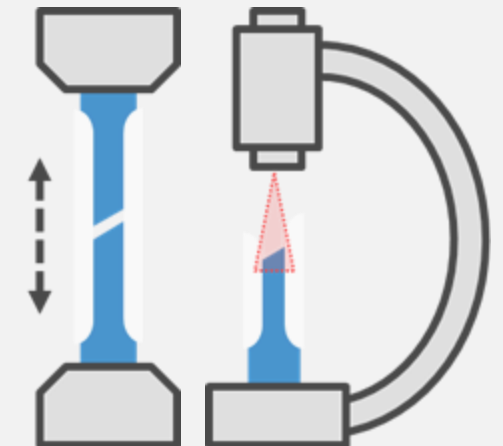
- Most ductile when untreated
- Fracture strain dropped after quenched

C. Annealed, Al-Si coated

- Most brittle after quenched
- Fracture strain dropped after quenched



**Fracture Strain
≠ Elongation**



Evolving Fracture Resistance of PHS1500|2000

GDIS

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From Untreated to
Quenched



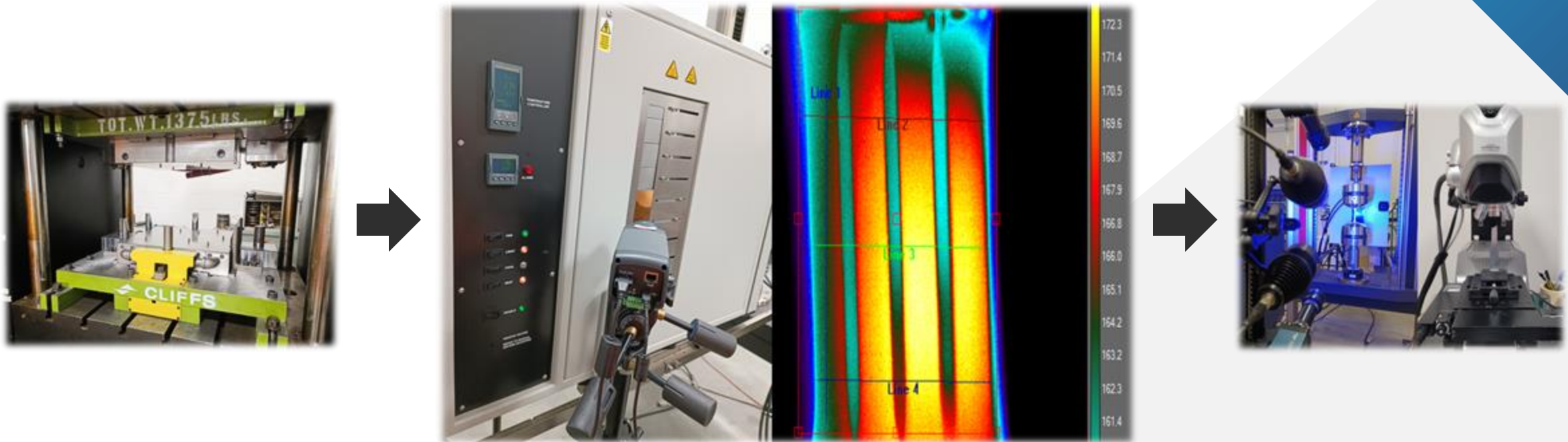
LTT (Paint-Baking) Effects



Rate / Stress-State Effects
(on Type-A)



LTT + Tensile Testing Procedure



LTT treatment: ASTM E8 tensile test samples were heat-treated in a temperature chamber (monitored by an infrared camera) to simulate the automotive paint-baking cycles

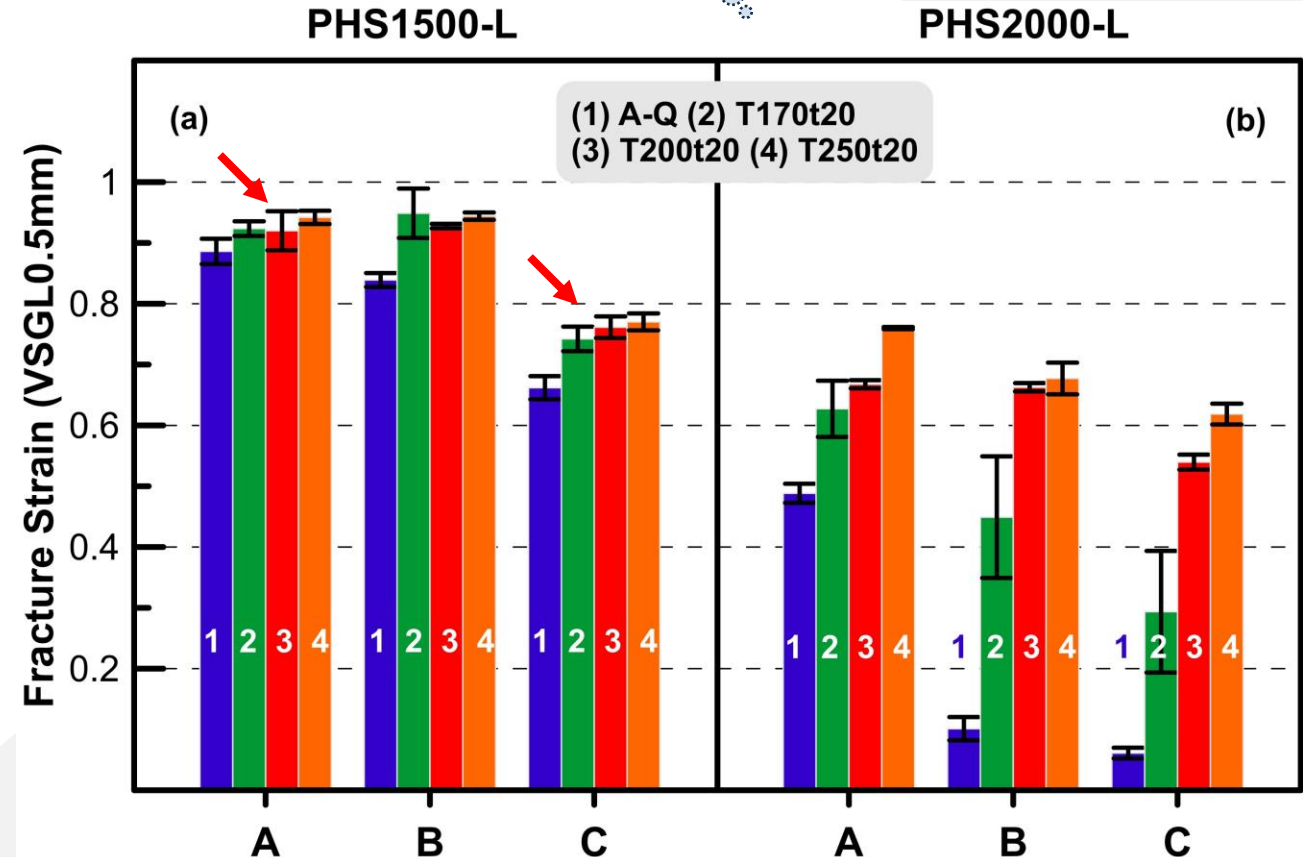
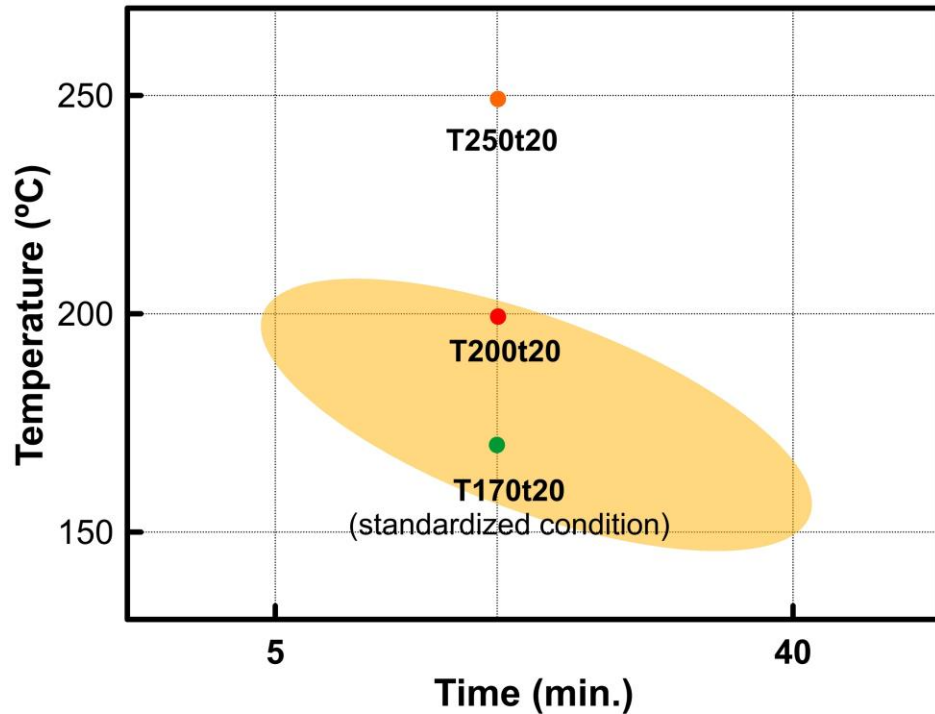
LTT-Elevated Tensile Fracture Strain Results

- A. Cold-rolled, uncoated PHS
- B. Annealed, uncoated PHS
- C. Annealed, Al-Si coated PHS

LTT improved PHS2000
more significantly
Higher temperature, higher elevation

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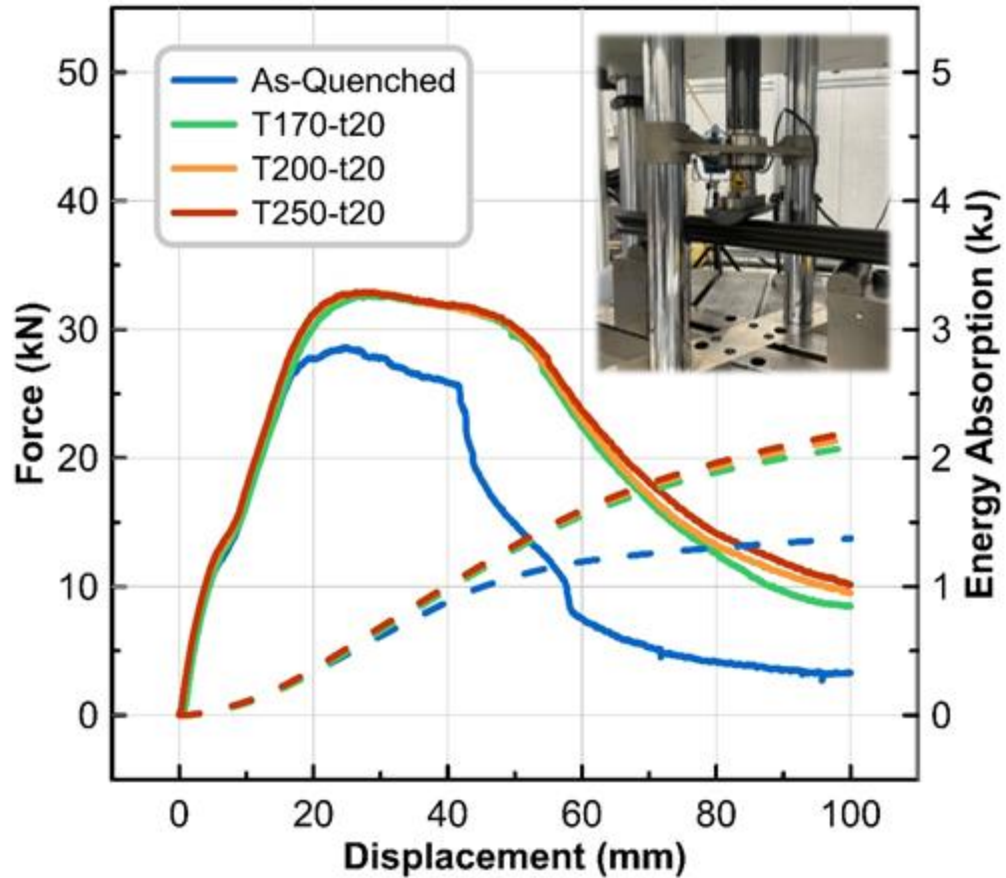
OEM-Provided Actual Paint-Baking Conditions



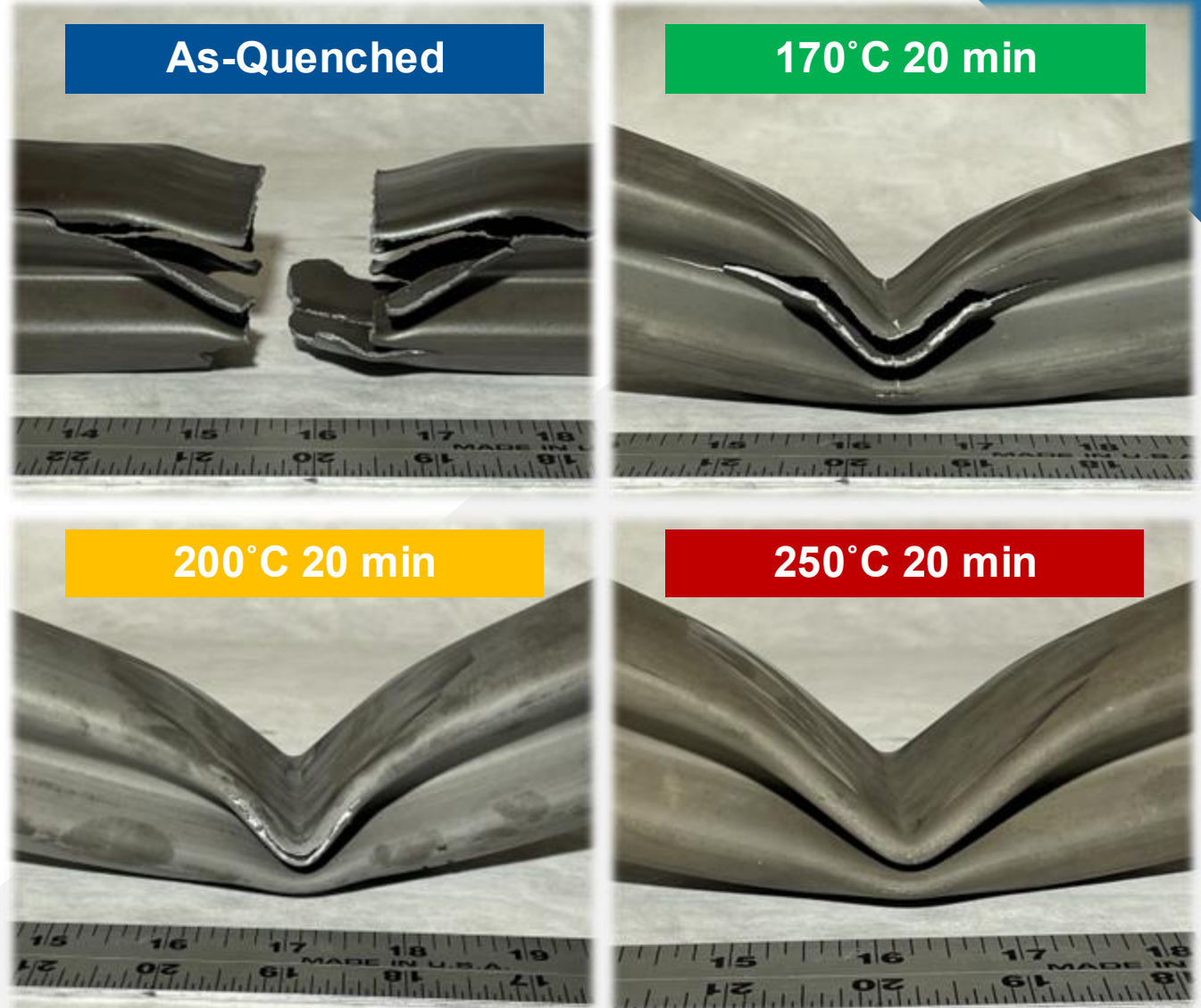
Cross-Validation with 3PB Results in GDIS 2024

GDIS

3PB on PHS1500 at 10 mm/s



Photos captured after delayed fracture



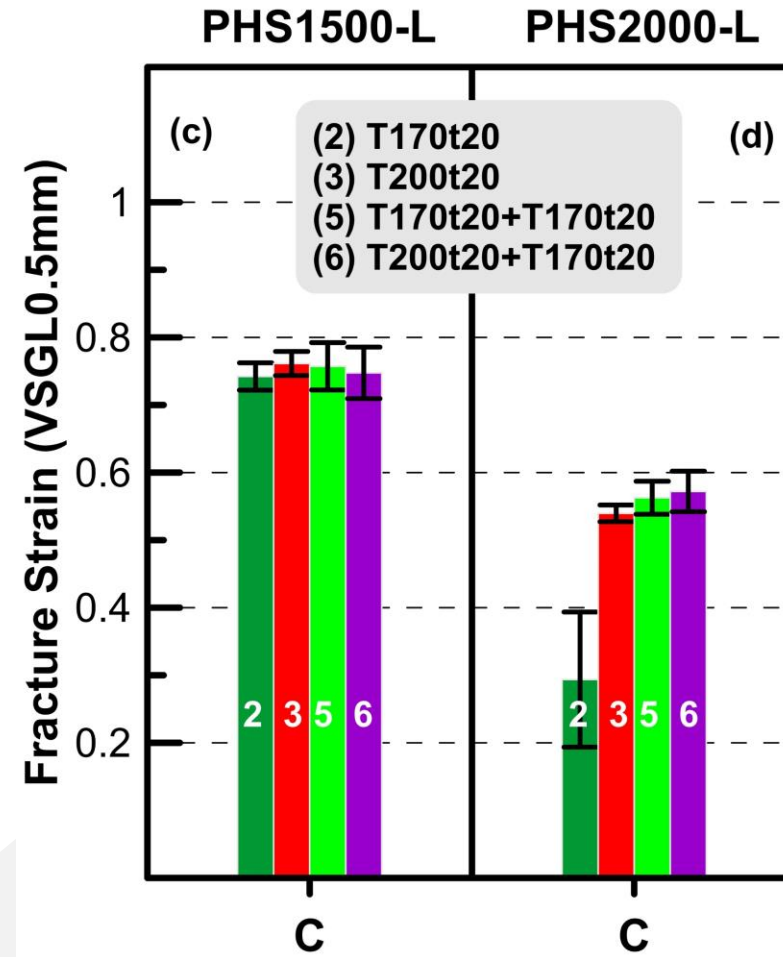
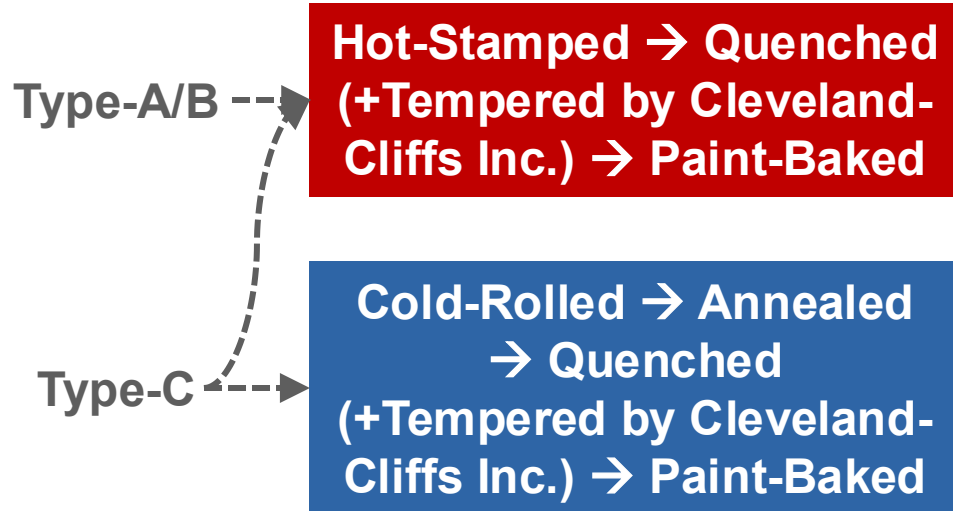
2x LTT + Tensile Testing Procedure



2x LTT treatment: to simulate a procedure of quenched PHS components being first tempered by Cleveland-Cliffs Inc. and then paint-baked in assembly by automakers; particularly applicable for Al-Si coated PHS (Type-C) tubular components

2x LTT-Elevated Tensile Fracture Strain Results

- A. Cold-rolled, uncoated PHS
- B. Annealed, uncoated PHS
- C. Annealed, Al-Si coated PHS



2x LTT effects
on fracture
strain saturated

Evolving Fracture Resistance of PHS1500|2000

GDIS

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From Untreated to
Quenched



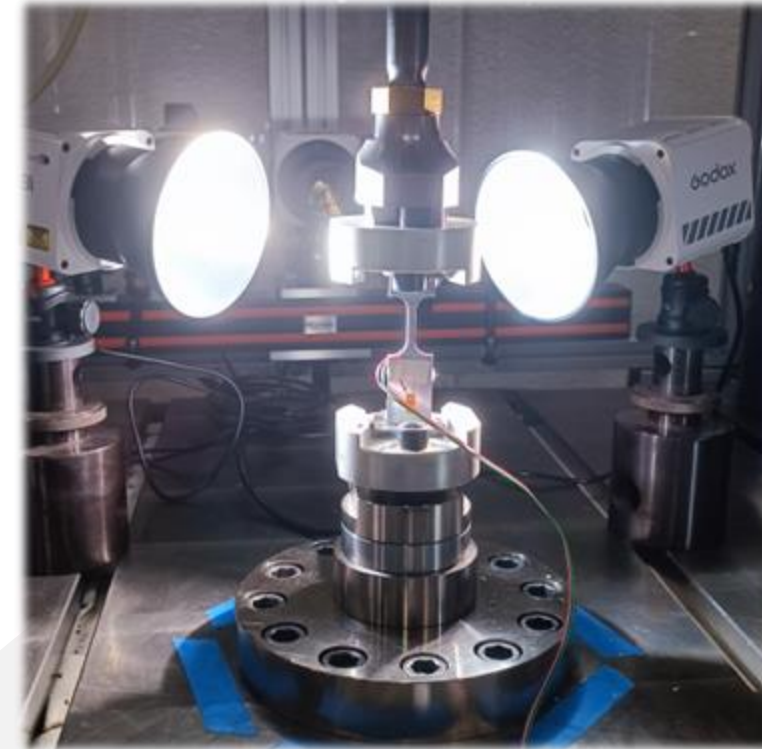
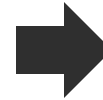
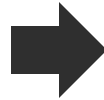
LTT (Paint-Baking) Effects



Rate / Stress-State Effects
(on Type-A)



Rate-Dependent Tensile Testing Procedure

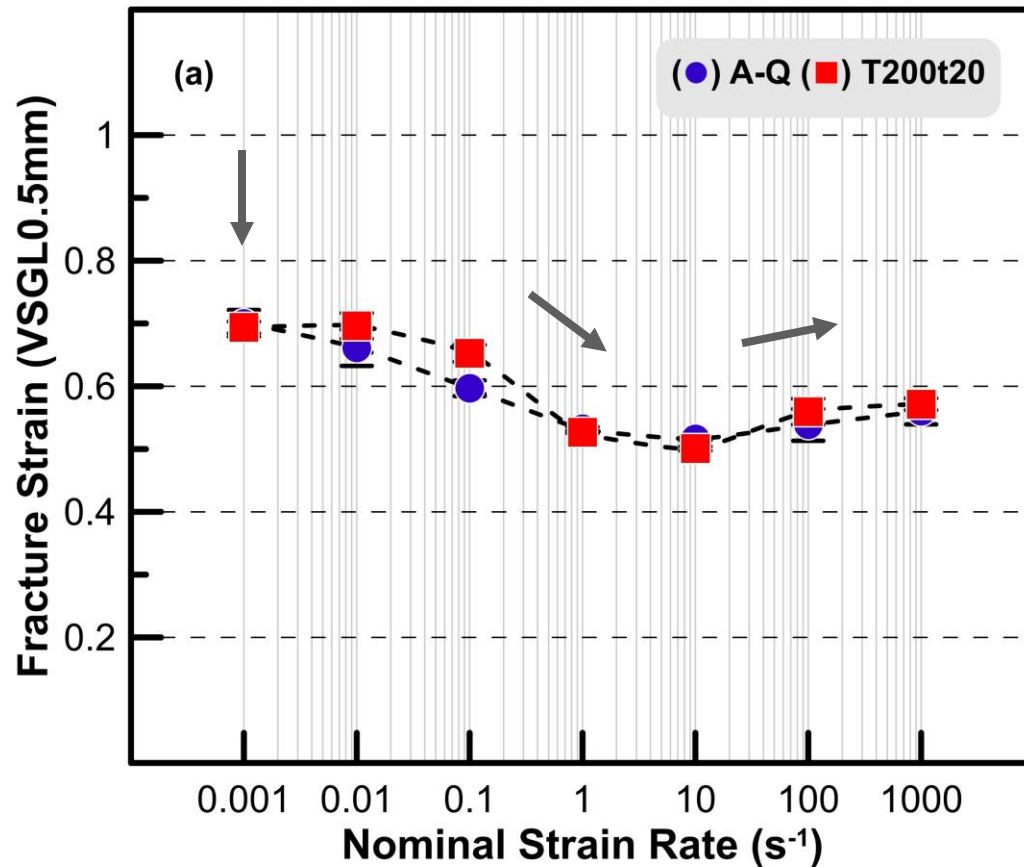


Rate-dependent tensile: as-quenched (A-Q) vs. T200t20-treated Type-A PHS1500|2000 samples were cut to modified ISO 26203-2 geometry and tested at $0.001 - 1000 \text{ s}^{-1}$ nominal strain rates and through fracture strain measurements

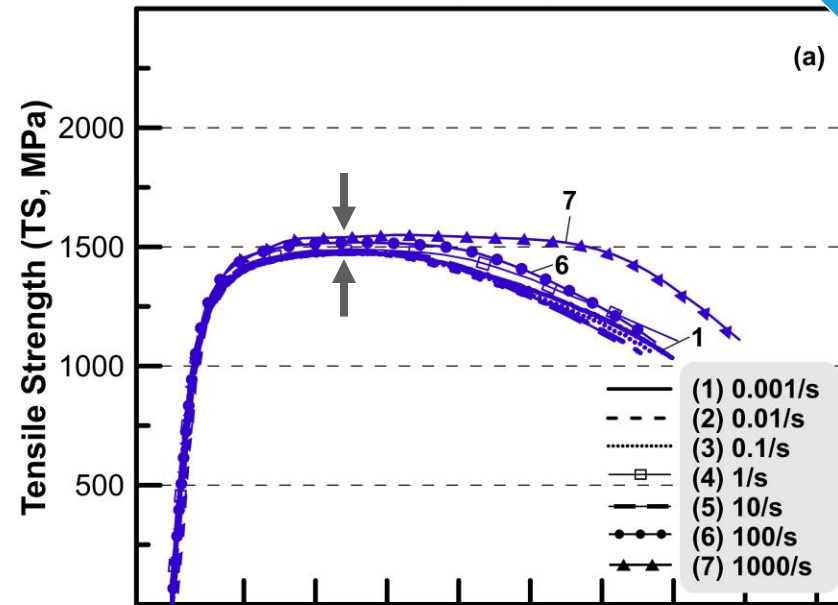
Results: PHS1500(A)

Effects of sample geometry, adiabatic heating & strain hardening

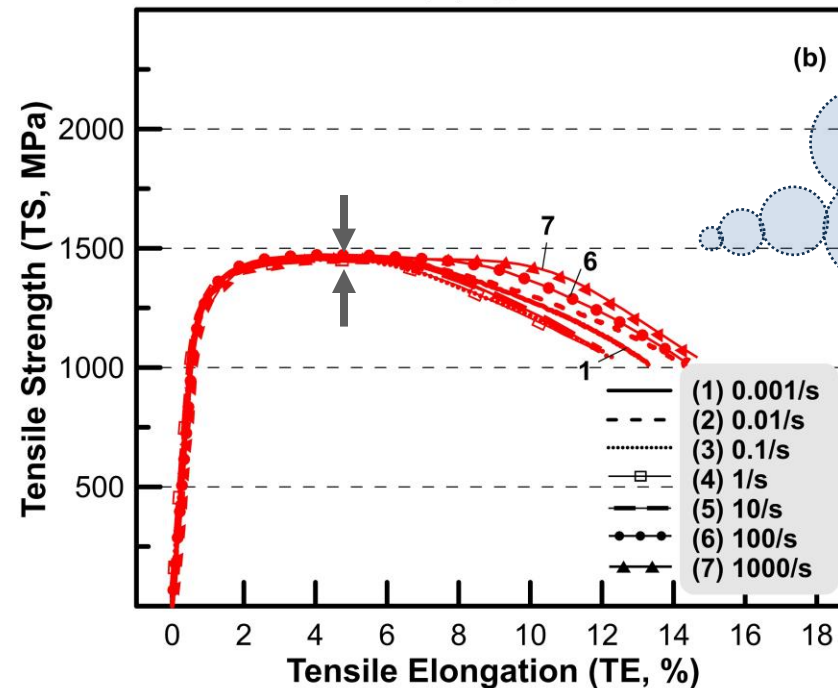
PHS1500(A)-L



PHS1500(A)-L_A-Q



PHS1500(A)-L_T200t20

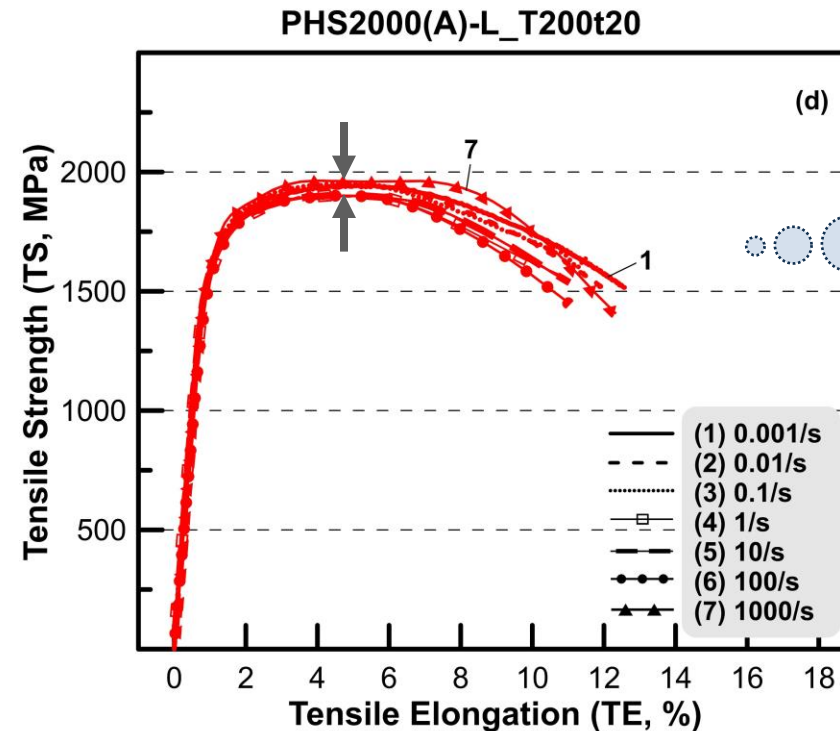
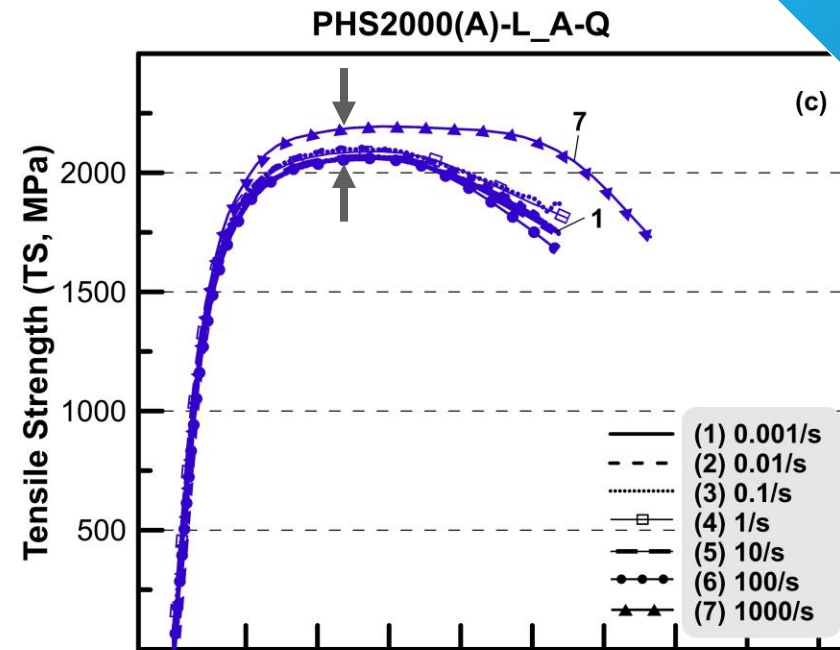
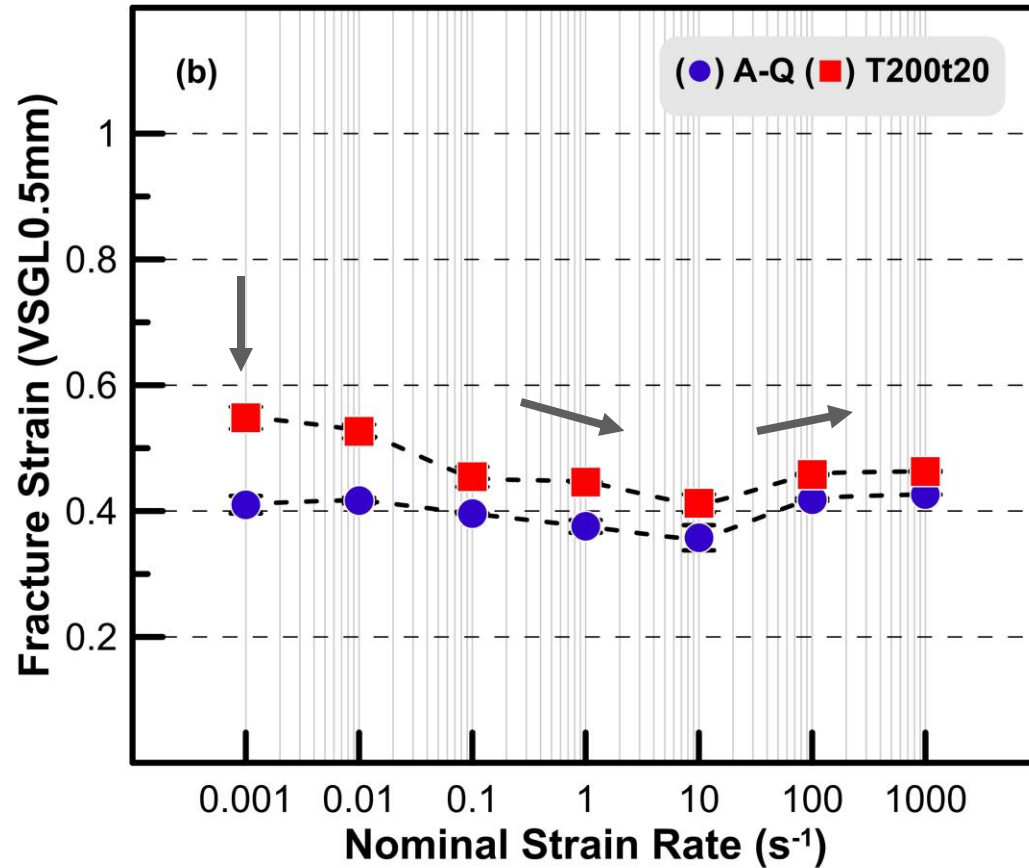


LTT decreased flow stress' rate sensitivity

Results: PHS2000(A)

Similar trends as
PHS1500(A)

PHS2000(A)-L

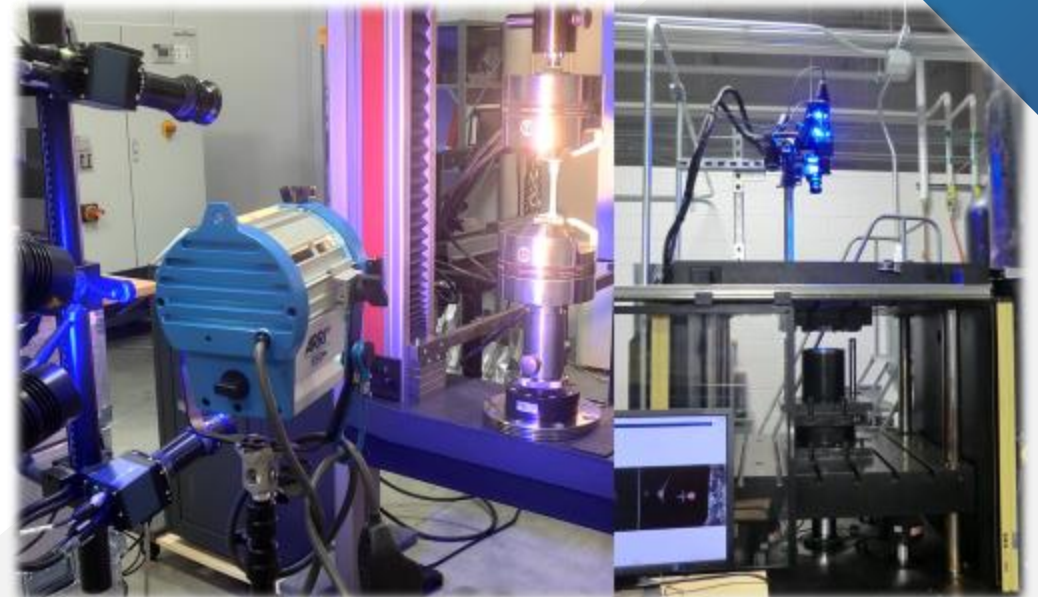
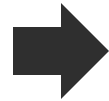


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Similar
trends as
PHS1500(A)

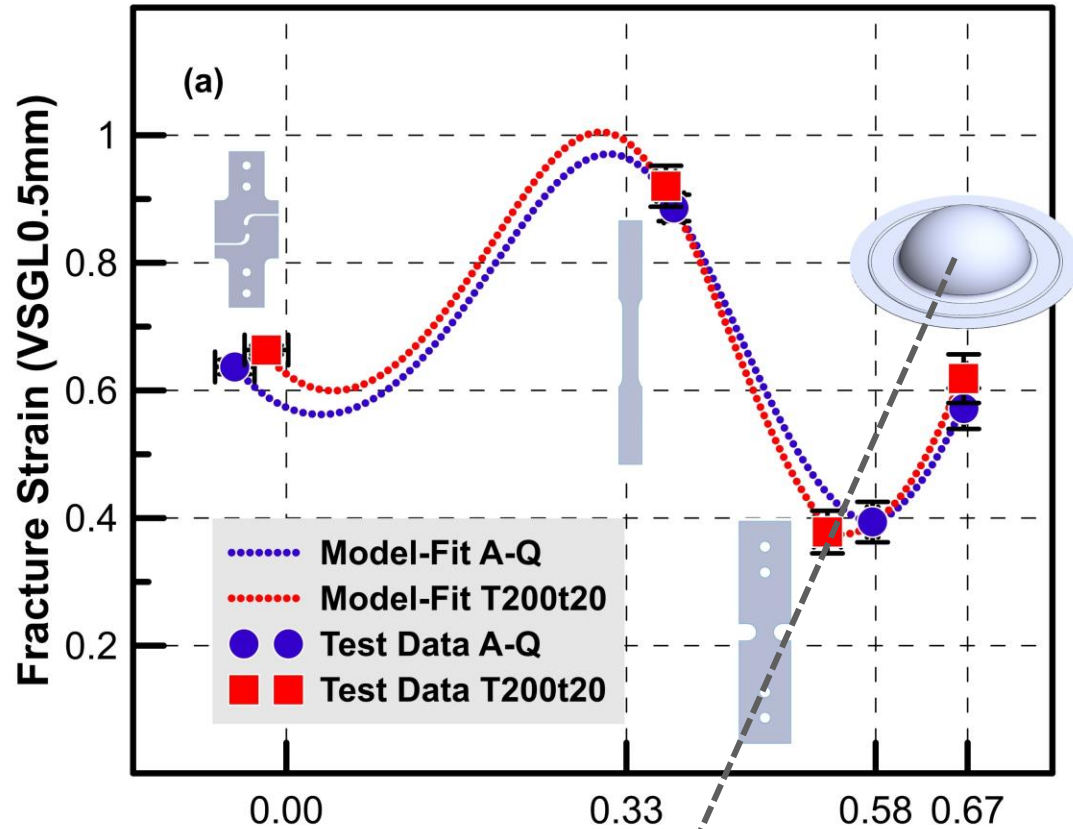
Stress-State-Dependent Testing Procedure



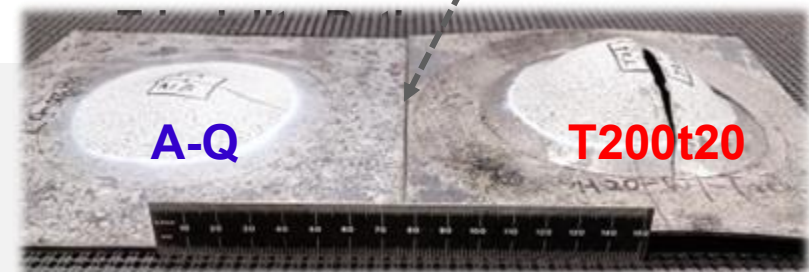
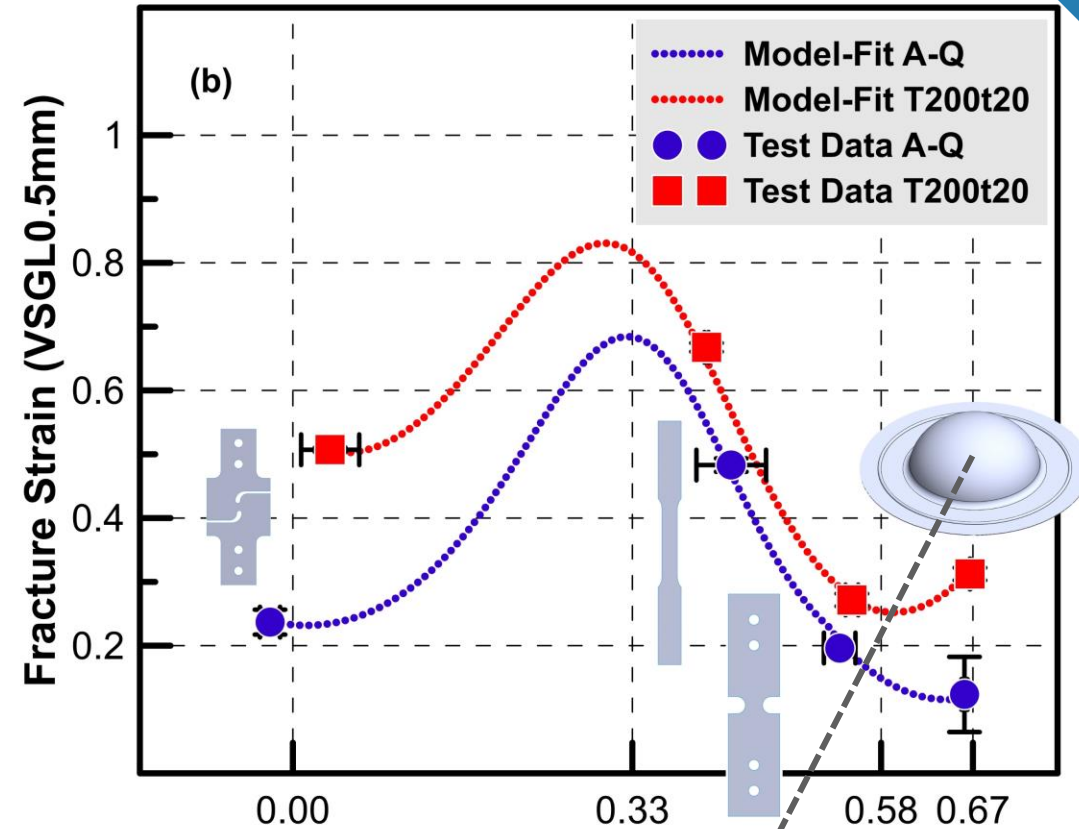
Stress states besides uniaxial tension: A-Q vs. LTT PHS1500|2000(A) samples were tested under quasi-static simple shear, plane strain, and equi-biaxial tension, and through fracture strain measurements

Stress-State-Dependent Fracture Strain Results

PHS1500(A)-L



PHS2000(A)-L



- ❖ **3 UHS-PHS types** exhibited distinct fracture resistance:
 - Type-A (cold-rolled, uncoated): most brittle when untreated, yet most ductile after quenched
 - Type-B (annealed, uncoated): most ductile when untreated
 - Type-C (annealed, Al-Si coated): most brittle after quenched
- ❖ **Low-temperature tempering (LTT)** could improve fracture resistance of quenched UHS-PHS:
 - LTT improved PHS2000 more significantly
 - Higher LTT temperature, higher fracture strain elevation
 - Longer LTT time (2x cycles), the elevation saturated
- ❖ **2 practical conditions** were evaluated on quenched vs. tempered PHS1500|2000(A):
 - Rate-dependent tensile tests revealed a common fracture-strain minimum near 10 s^{-1} due to competing strain hardening and adiabatic heating; LTT reduced rate sensitivity of flow stress and enhanced fracture strain, especially for PHS2000(A)
 - Stress-state-dependent tests confirmed that LTT increased fracture strain across all stress states for PHS2000(A), with the most pronounced gains under simple shear and equi-biaxial tension

THANK YOU!

For More Information



Jun Hu, PhD

Jun.Hu@clevelandcliffs.com

Laura Burroughs

Laura.Burroughs@clevelandcliffs.com

Grant Thomas, PhD

Grant.Thomas@clevelandcliffs.com

Relevant publications:

- **On Fracture Resistance of Ultra-High-Strength Press-Hardened Steels, *AIST 3rd Auto Steel Int. Conf. 2025***
- **Influence of Low-Temperature Tempering on Mechanical Behavior of a Press-Hardened 22MnB5 Steel Grade, *CHS² 2024***
- **On Local Formability/Ductility of New Advanced High-Strength Steels: Temperature, Bake Hardening, and Strain Rate Effects, *AIST Transactions 2024***
- **True Fracture Strain Measurement and Derivation for Advanced High-Strength Steel Sheets, *SAE 2022, GDIS 2023***