



UNIVERSITY OF  
**WATERLOO** | FACULTY OF  
ENGINEERING

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# Advancing LME Understanding: Standardized Characterization and Direct Observation in Resistance Spot Welding

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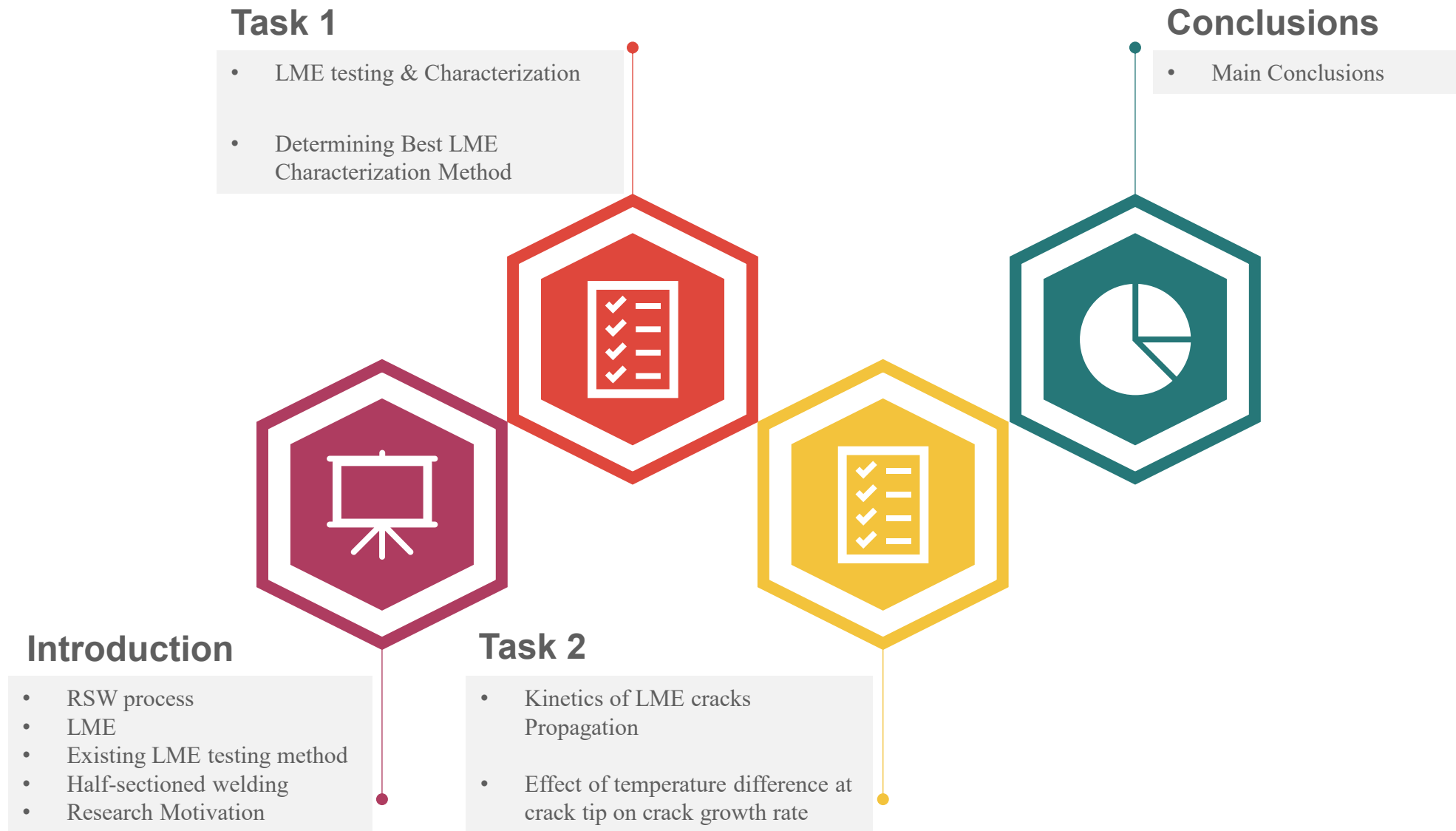
<sup>1</sup>Department of Mechanical and Mechatronics Engineering, University of Waterloo, Waterloo, ON, Canada;

<sup>2</sup>General Motors R&D, Manufacturing Systems Research Laboratory, Michigan, USA

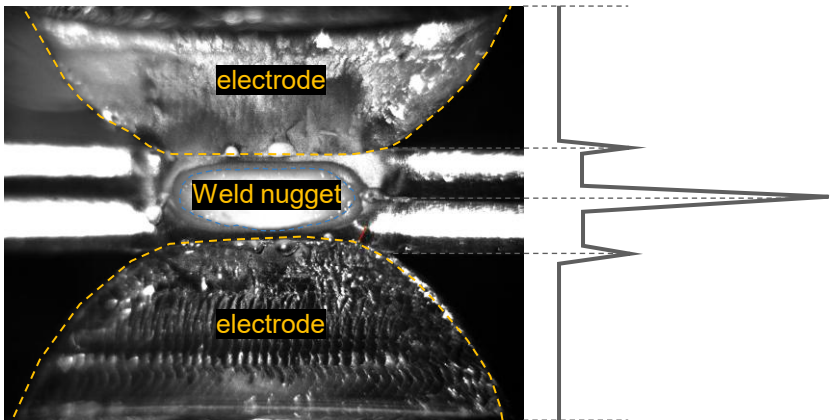


Auto/Steel  
Partnership

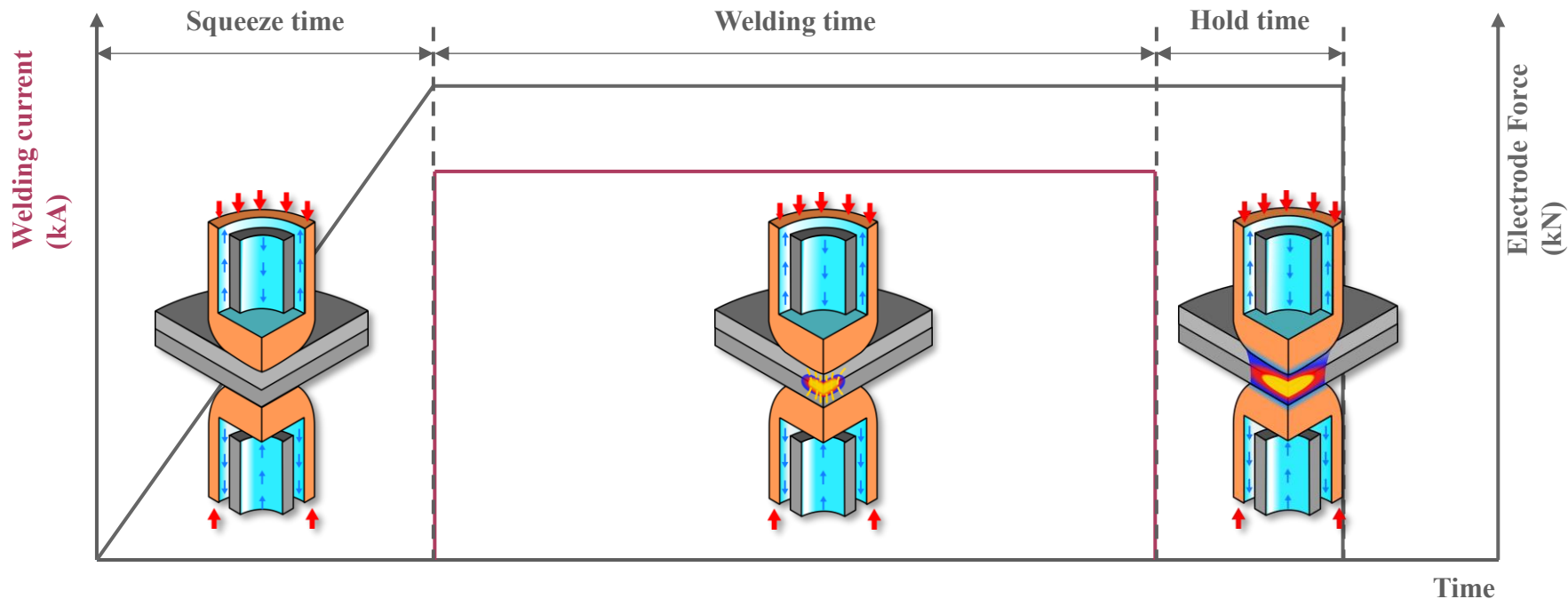
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# Resistance Spot Welding Process

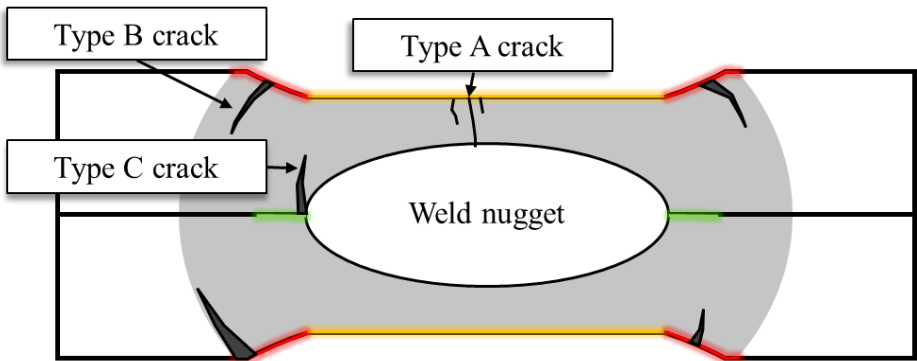
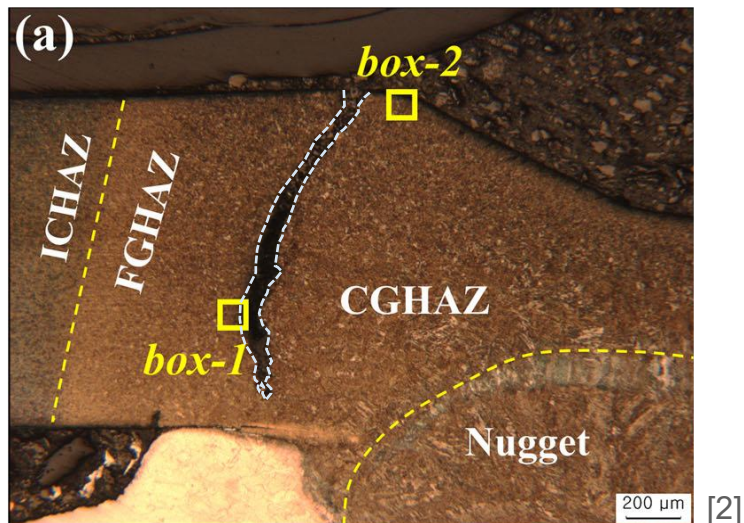
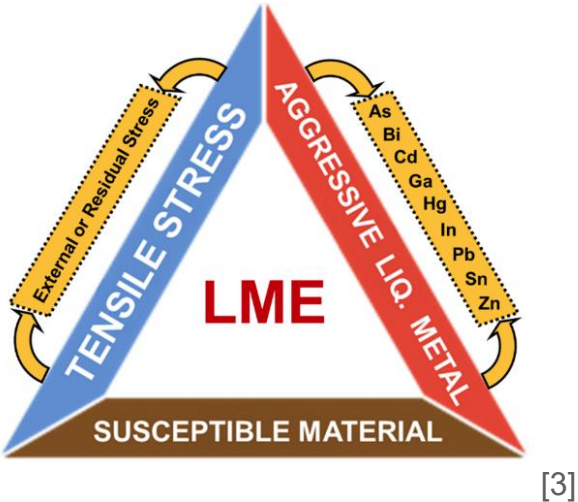
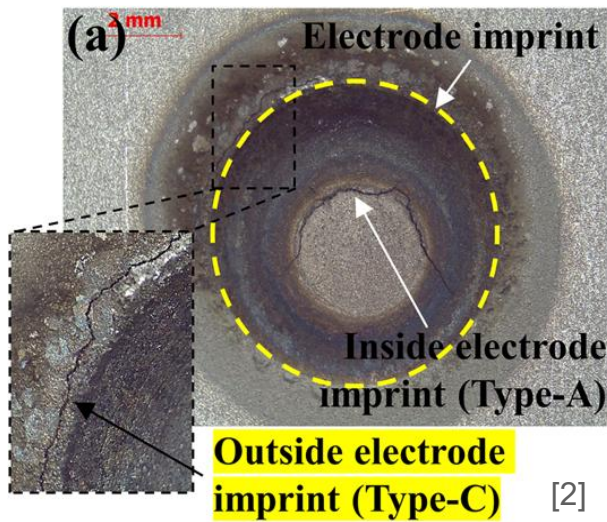


$$Q \text{ (heat)} = \int_0^t I^2(t)R(t)dt$$



[1] Resistance spot welding link: <https://youtu.be/N5AYZxsnDuM?si=hTD7jHQTcOVbXDUQ>

# Liquid Metal Embrittlement (LME)



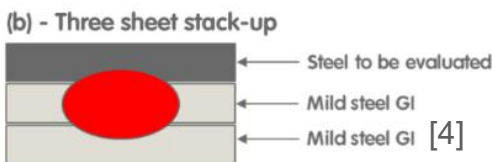
[2] Murugan, S. P., et al. Liquid Zinc penetration induced intergranular brittle cracking in resistance spot welding of galvanized advanced high strength steel. *Welding in the world*. (2020) 64:1957-1969.  
[3] Razmpoosh, M. et al. Pathway to understand liquid metal embrittlement (LME) in Fe-Zn couple: From fundamentals toward application. *Progress in Materials Science* (2021) 121.

# LME Testing and Characterization Methods

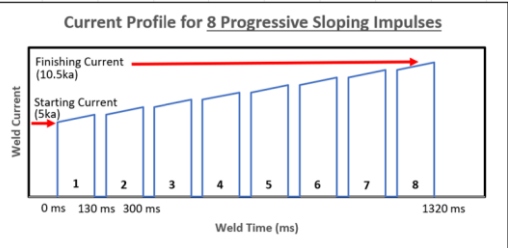
## Testing



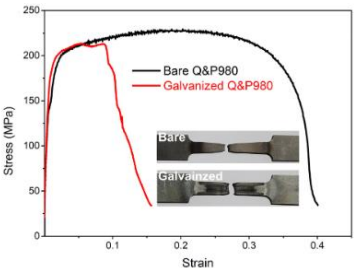
2-High Spot Welds



3-High Spot Welds

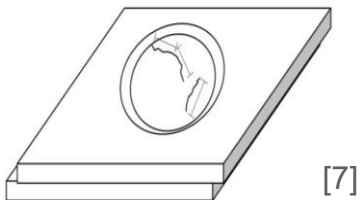


A/SP Rapid LME Test



Hot Tension Testing (Gleeble)

## Characterization

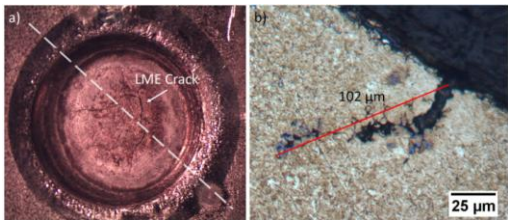


Surface Crack Measurement

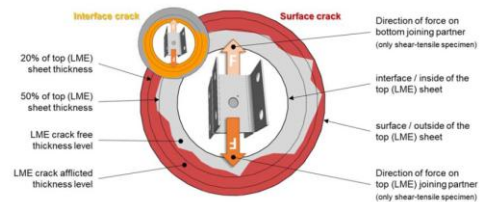
| 4 Crack Types by Relative Temperature: |                       |                      |                          |                            |
|----------------------------------------|-----------------------|----------------------|--------------------------|----------------------------|
|                                        | Type A                | Type B               | Type C                   | Type D                     |
| Relative Test Current                  | High Temp LME (>650C) | Low Temp LME (<650C) | Interfacial LME (? rare) | Threshold Temp LME (~650C) |
| Below Expulsion                        | > 10%                 | > 5%                 | > 5%                     | > 5%                       |
| At (or above) Expulsion                | NOK                   | NOK                  | NOK                      | NOK                        |
|                                        | OK                    | NOK                  | NOK                      | NOK                        |

[5]

Cross-section Crack Classification



Cross-section Crack Measurement



Computed tomography (CT) Scanning

There is no standardization in testing or LME severity metrics

[4] D. Benlatreche et al., The 72nd annual assembly of the International Institute of Welding (IIW) (2019).

[5] M. Karagoulis, General Motors, (2019).

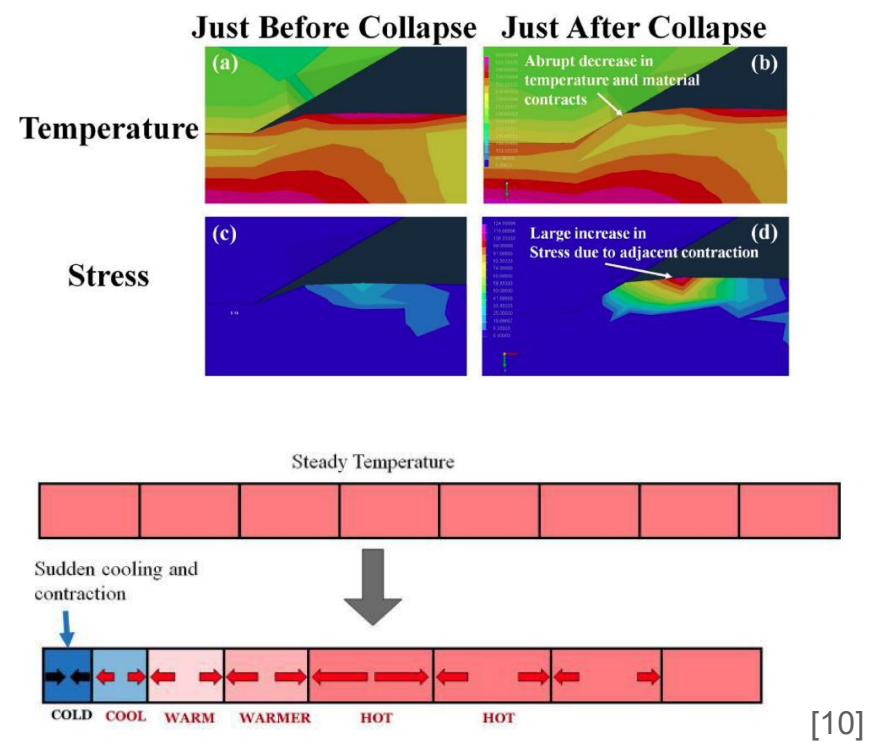
[6] Z. Ling et al., Materials & Design, (2020).

[7] E. Tolf et al., Science and Technology of Welding and Joining, (2013).

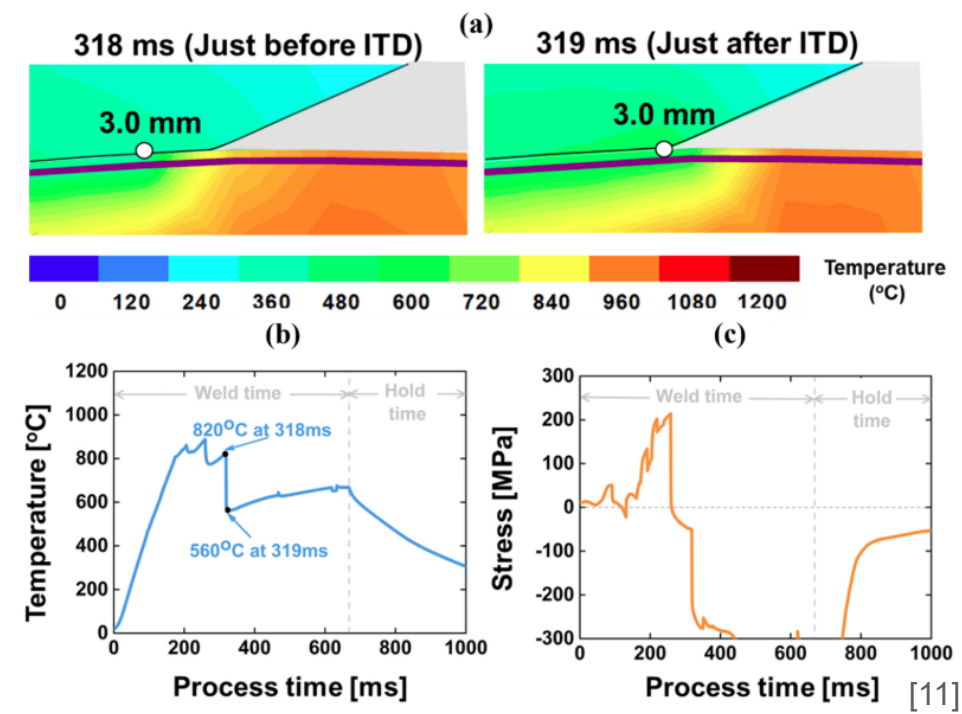
[8] E. Wintjes et al., Welding in the World, (2019).

[9] G. Meschut et al., World Auto Steel, (2020).

# Thermal Stress Development at the Weld Shoulder



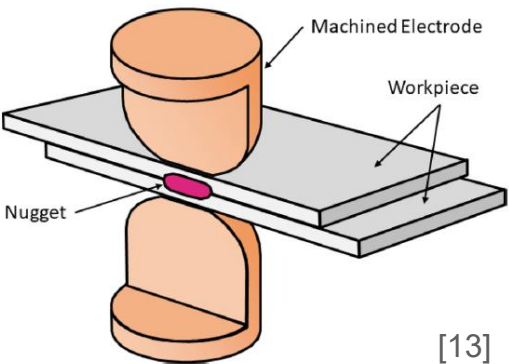
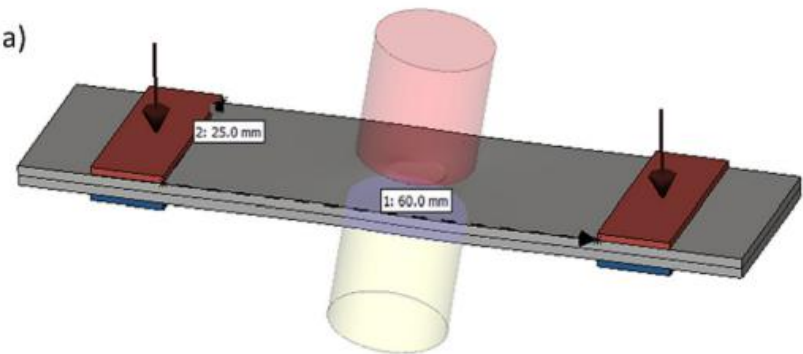
Electrode-to-sheet contact induces an instantaneous temperature drop (ITD), causing thermal stress



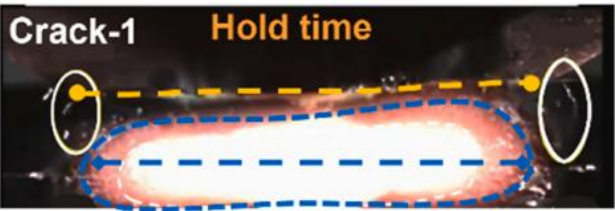
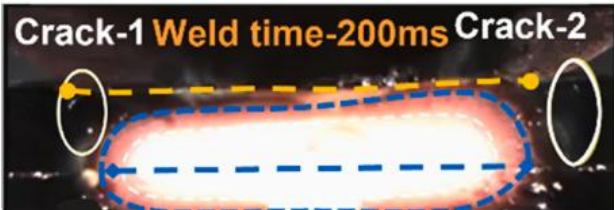
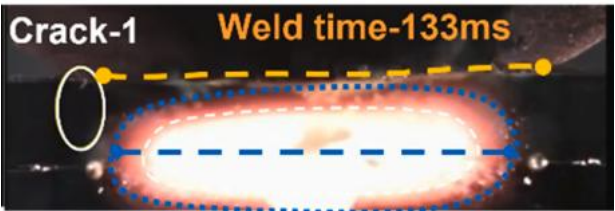
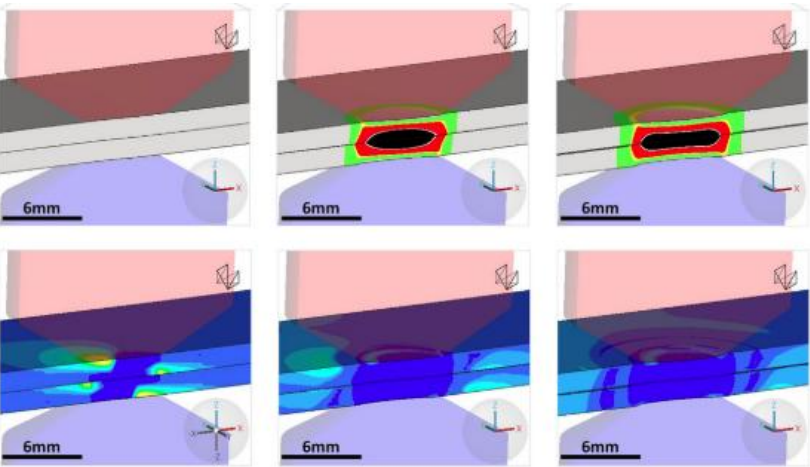
Thermal stress plays a dominant role in LME crack during the RSW process

[10] DiGiovanni G. et al. Role of spot weld electrode geometry on liquid metal embrittlement crack development. Journal of Manufacturing Processes (2020) 49:1-9  
[11] Lalachan A. et al. Liquid metal embrittlement in Zn-coated steel resistance spot welding: Critical electrode-contact and nugget growth for stress development and cracking. (2023) 318.

# Half-Sectioned Resistance Spot Welding (H-RSW)



[13]



[11]

**No Quantitative analysis on LME crack during the actual spot-welding environment**

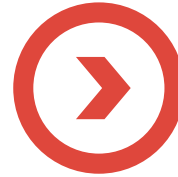
[11] Lalachan A. et al. Liquid metal embrittlement in Zn-coated steel resistance spot welding: Critical electrode-contact and nugget growth for stress development and cracking. (2023) 318.  
[12] Okigami, F. et al. Numerical modeling of liquid metal embrittlement initiation during resistance spot welding of third generation advanced high strength steel-Effect of welding schedule and electrode alignment. Journal of Manufacturing Processes. (2024) 110:173-191.  
[13] Brizes, E. et al. Evaluation of heat transfer within numerical models of resistance spot welding using high-speed thermography. Journal of Materials Processing Technology. (2021) 297

## Goals of each task

- Task 1:



Since there is **no standardization** in LME testing or severity metrics, so current data cannot be compared



A **standard LME testing** and **measurement methodology** must be developed to compare LME severity results to both each other and to expected results during manufacturing

- Task 2:



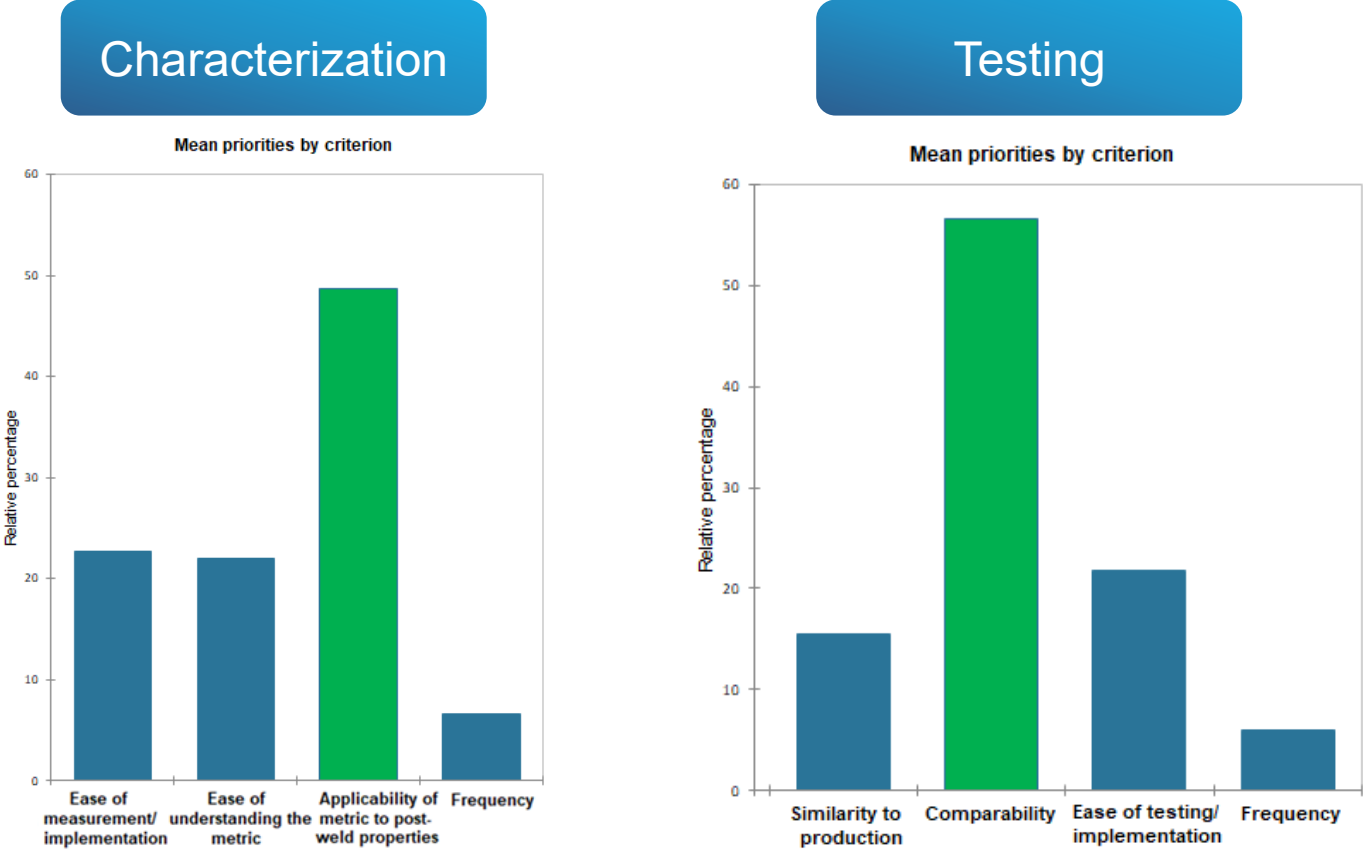
What are the **growth kinetics** (e.g., crack growth rate) and **key factors** controlling LME crack propagations?



**Quantitative analysis** on LME crack **propagation** using various electrode geometries to determine key factors controlling LME crack propagation.

# Testing and Characterization Comparison

Testing and characterization procedures were evaluated using both the **Delphic Hierarchy Process** and the **Analytic Hierarchy Process**. These methods were used to compare various methodological options and identify which test should be considered.



# LME Characterization Option Priorities

| Type of metric    |
|-------------------|
| Qualitative       |
| Quantitative      |
| Semi/quantitative |

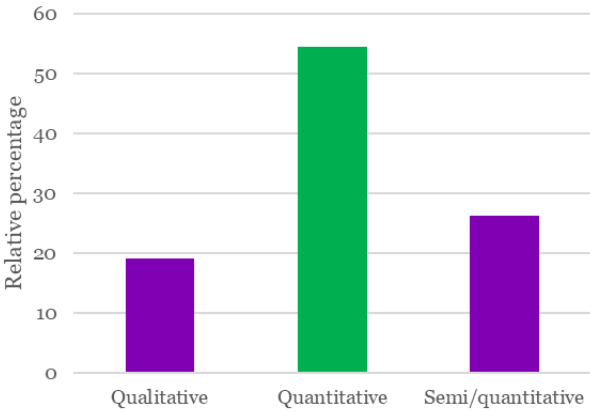
| Definition of metric                    |
|-----------------------------------------|
| Cracking index                          |
| Maximum (average) crack depth (length)  |
| Number (frequency) of cracks            |
| Surface cracking                        |
| Crack free welding parameters (current) |
| Percentage of cracked welds             |
| Crack/no crack                          |
| Crack location                          |
| A model (based on ductility lost)       |

| Characterization method |
|-------------------------|
| Surface cracking        |
| Cross-sectioning        |
| NDT                     |

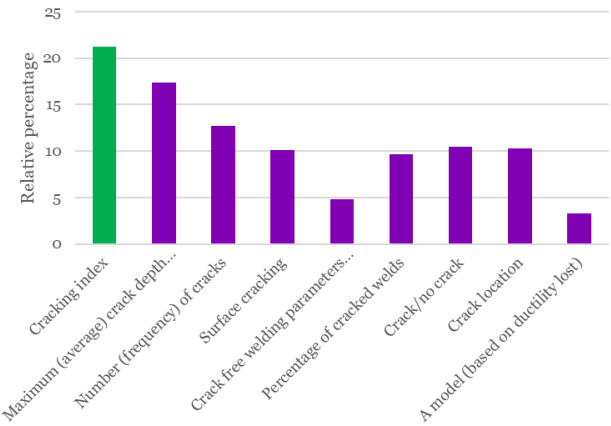


Increasing the priority of alternatives

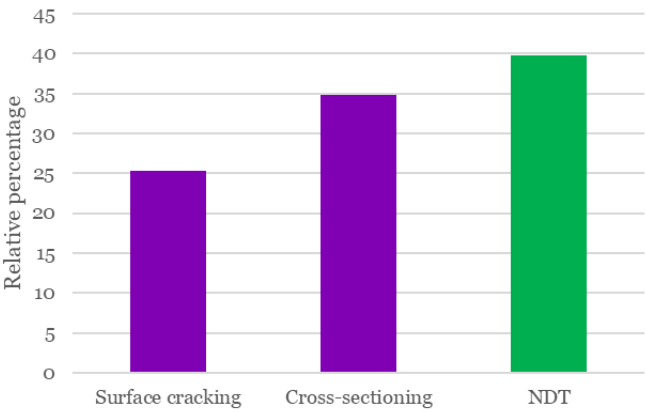
Mean priorities of alternative



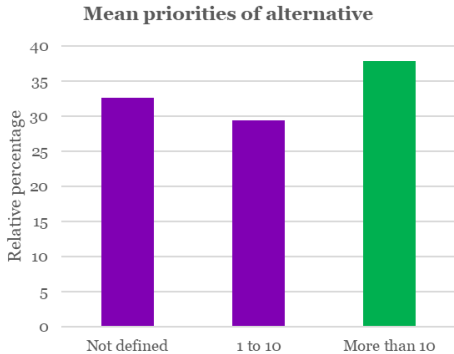
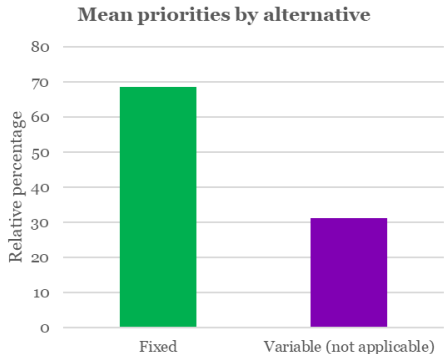
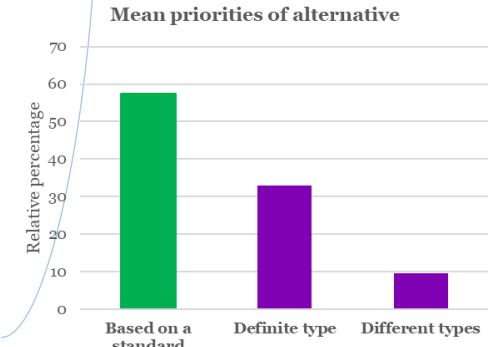
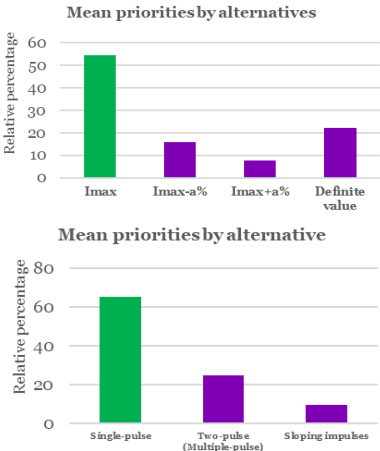
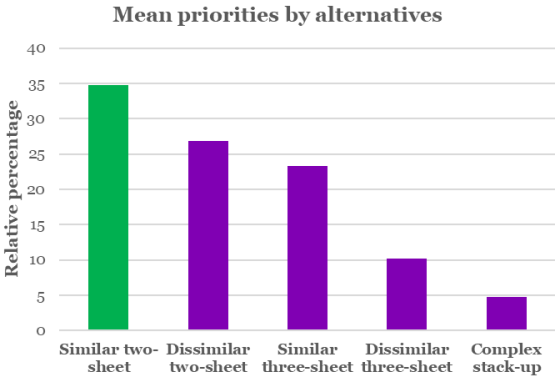
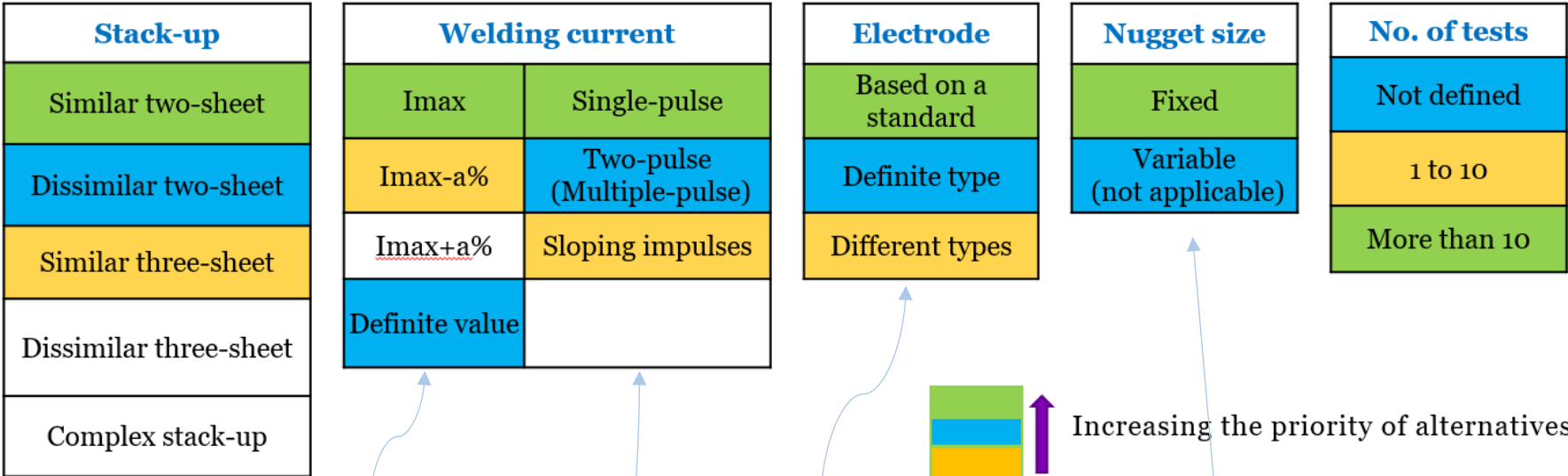
Mean priorities by alternative



Mean priorities by alternative



# LME Testing Option Priorities



# Results of Testing and Measurement Comparisons



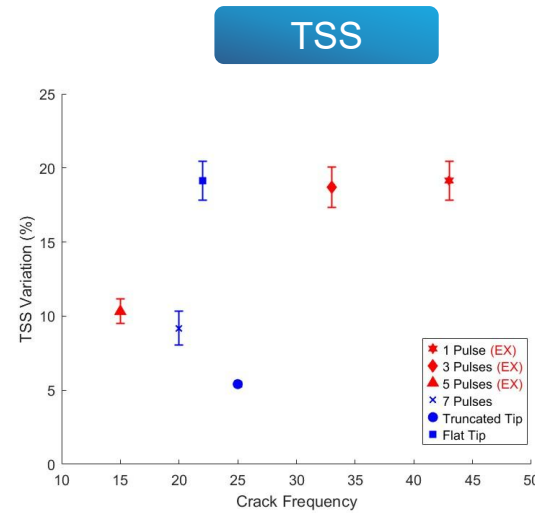
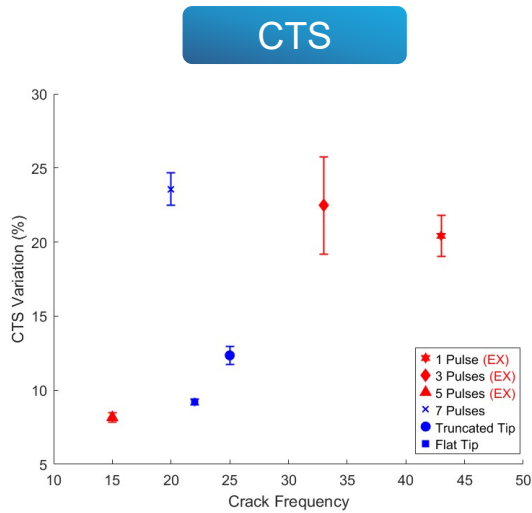
|                                   | Type of metric | Definition of metric | Characterization method |
|-----------------------------------|----------------|----------------------|-------------------------|
| LME characterization alternatives | Quantitative   | Cracking index       | Cross-sectioning        |

|                          | stack-up          | welding current  |              | Electrode           | Nugget size | No. of tests |
|--------------------------|-------------------|------------------|--------------|---------------------|-------------|--------------|
| LME testing alternatives | Similar two-sheet | I <sub>max</sub> | Single-pulse | Based on a standard | Fixed       | More than 10 |

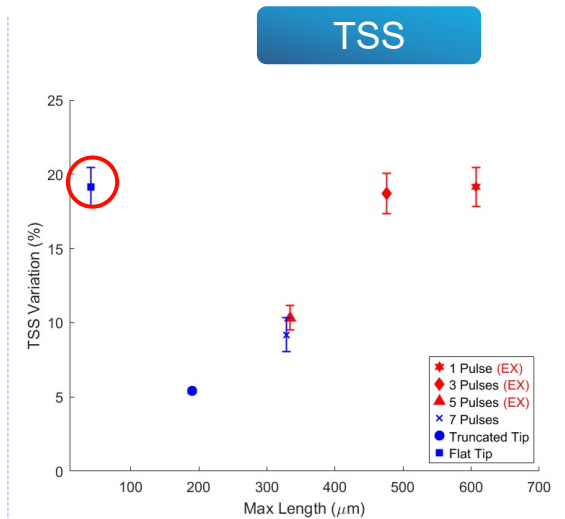
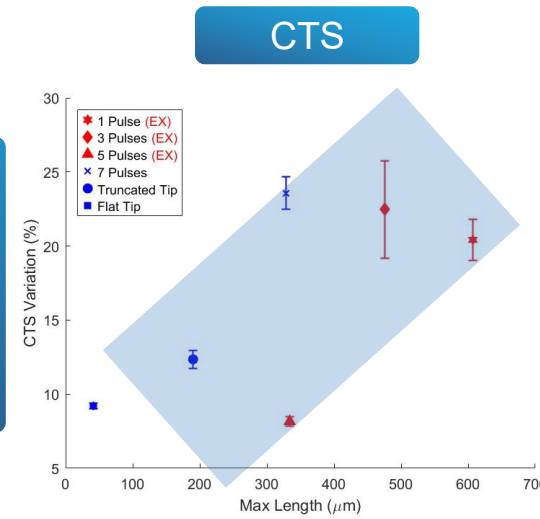
# Determining Best LME Characterization Method

## Correlation of Cracking and Welding Strength – Maximum Crack Length, Average Crack Length, and Crack Frequency

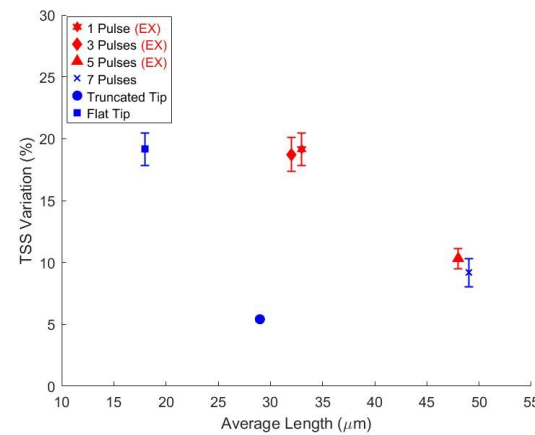
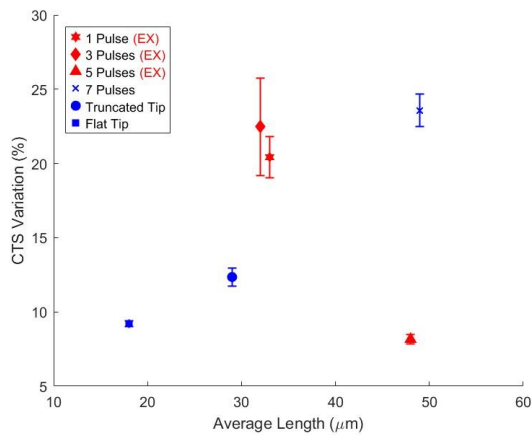
Crack Frequency



Max Length



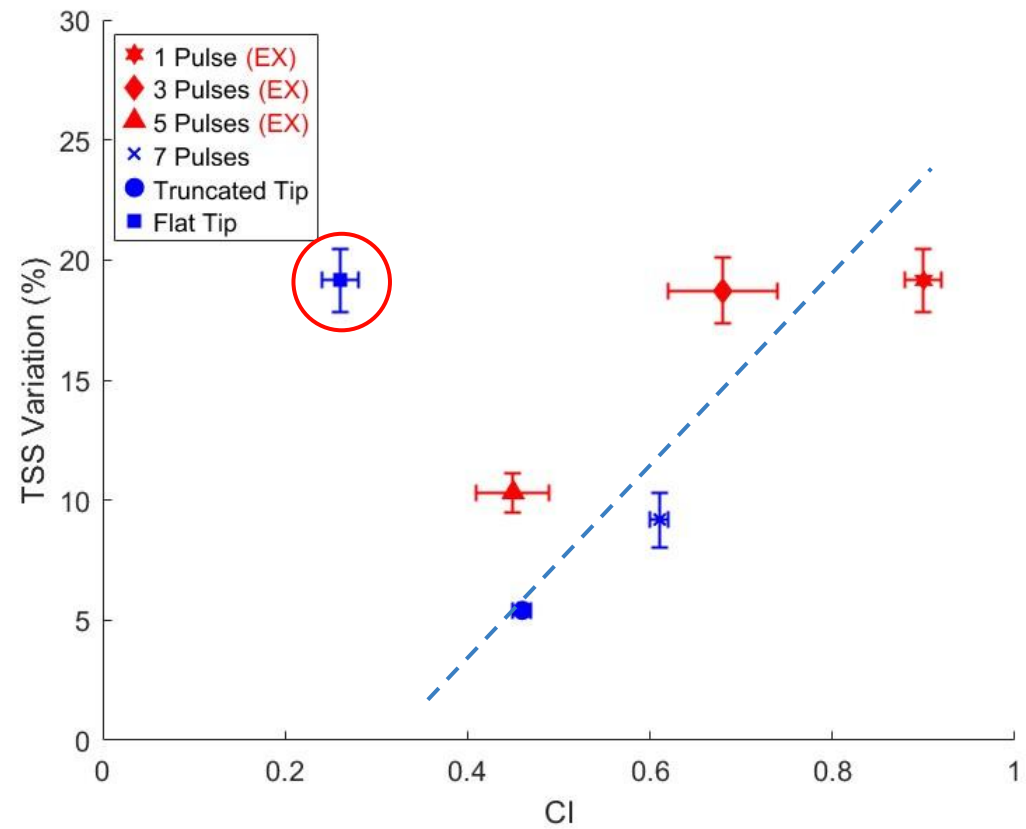
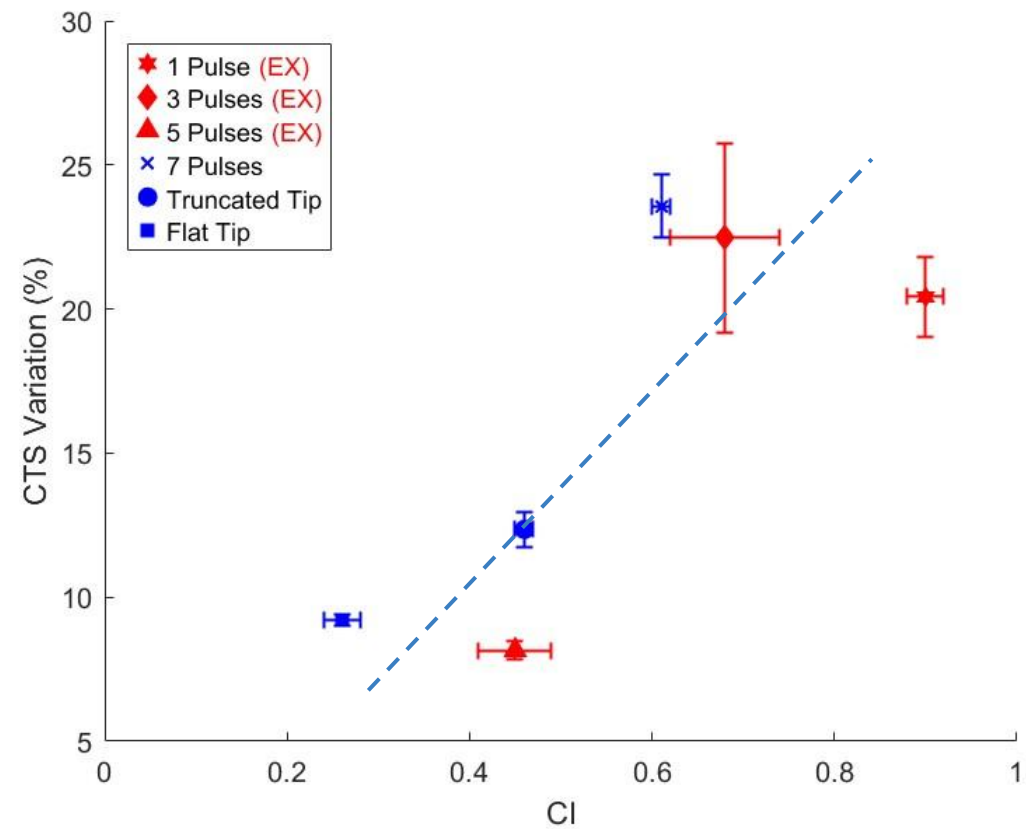
Average Length



- Crack frequency is a poor indicator of CTS and TSS.
- Average crack length is a poor indicator of CTS and TSS; TSS increases with average crack length.
- Max crack length is a good indicator of TSS, but there is a wide spread of the CTS data.

# Determining Best LME Characterization Method

## Correlation of Cracking and Welding Strength – Cracking Index



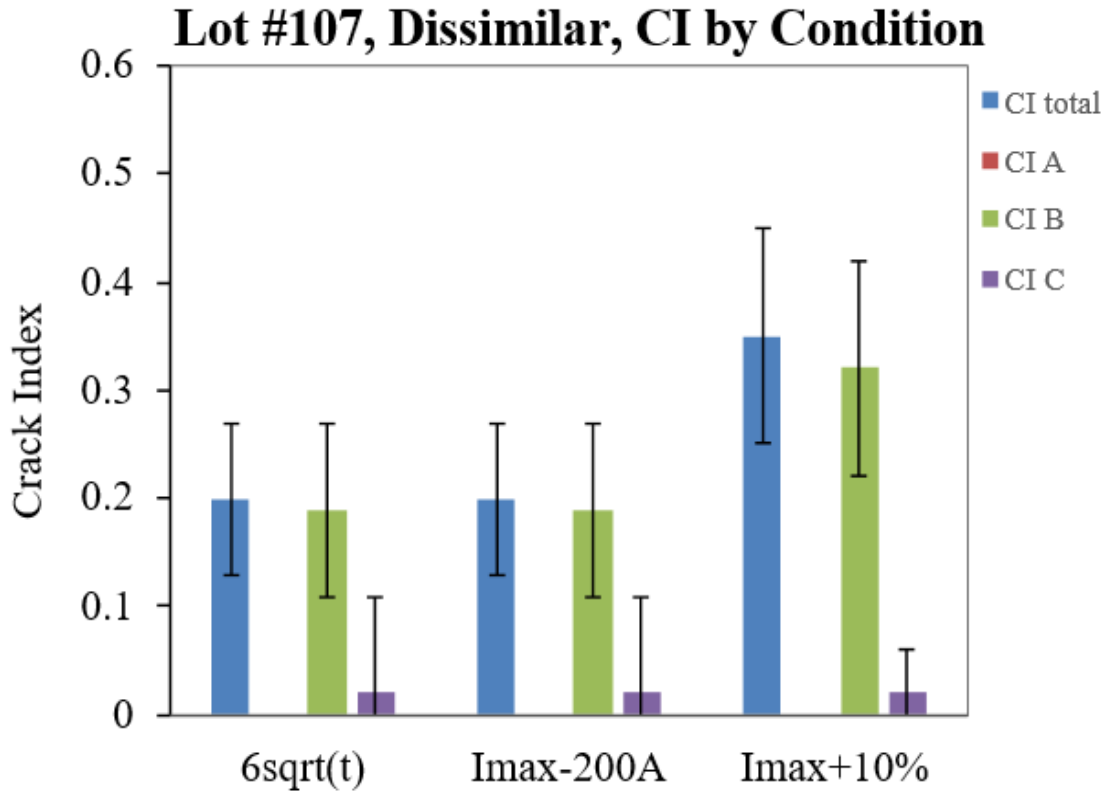
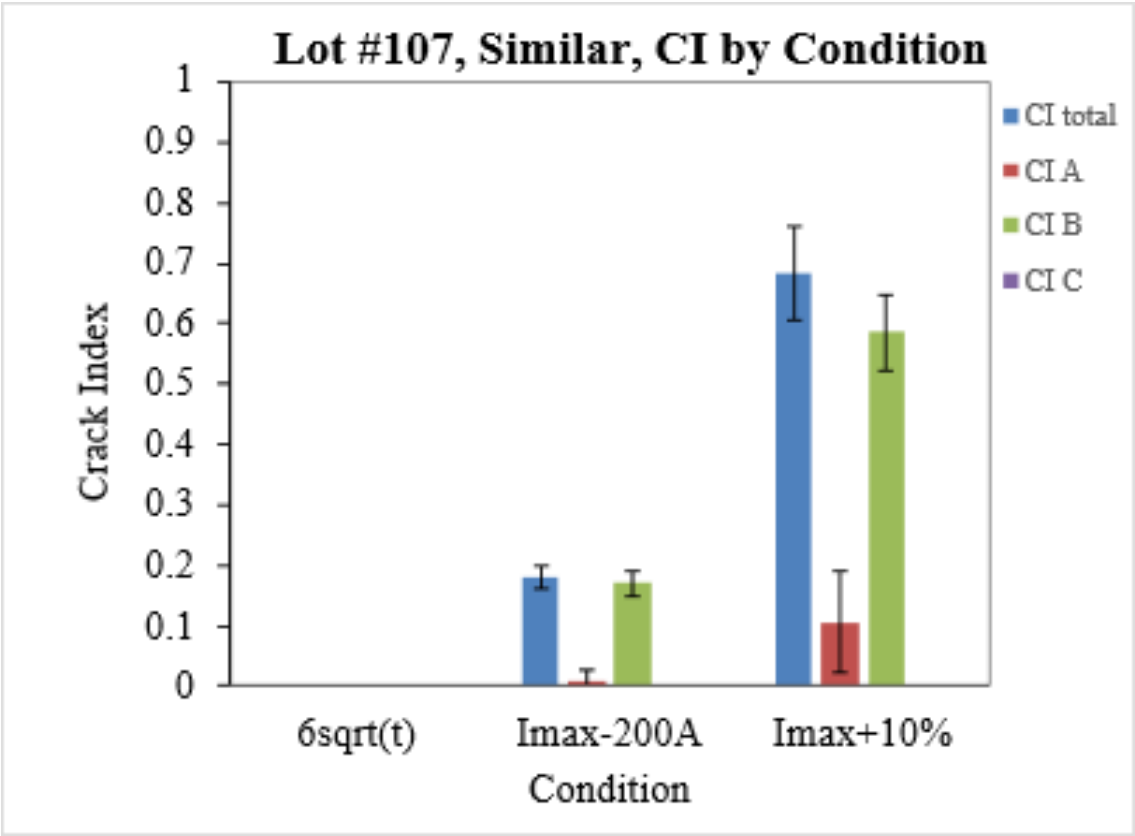
**Cracking Index is a good Indicator or CTS and TSS**

\*CTS: Cross tensile strength  
\*TSS: Tensile shear strength

# Crack Index Method Validation



Similar/dissimilar stack-up comparison/effect of current level on LME susceptibility



$I_{min}$ : Current meet minimum requirement of nugget size ( $6\sqrt{t}$ )  
 $I_{max}$ : highest current at which no expulsion occurs in ten consecutive welding trials

# Crack Index Method Validation

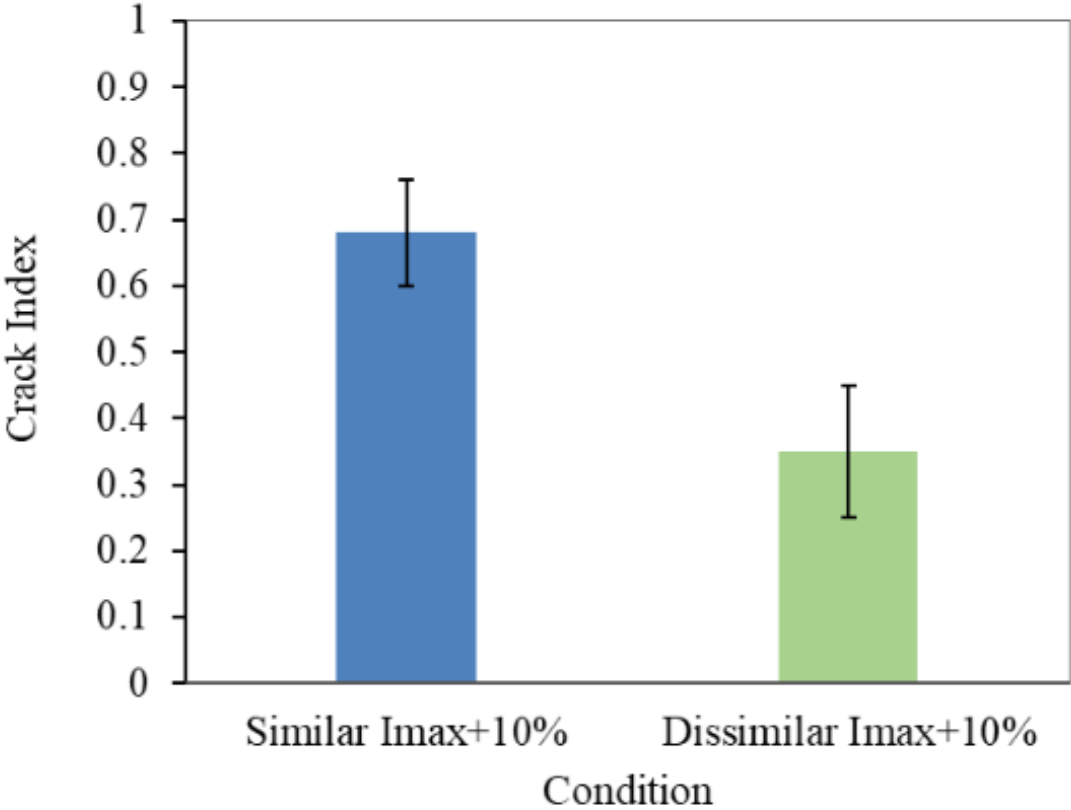
Similar/dissimilar stack-up comparison/effect of current level on LME susceptibility



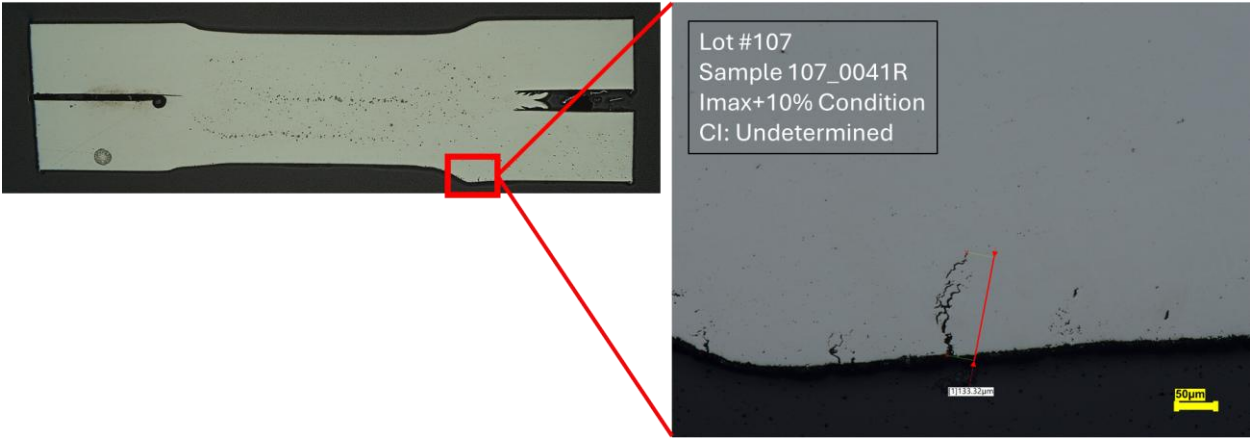
← Similar stack-up



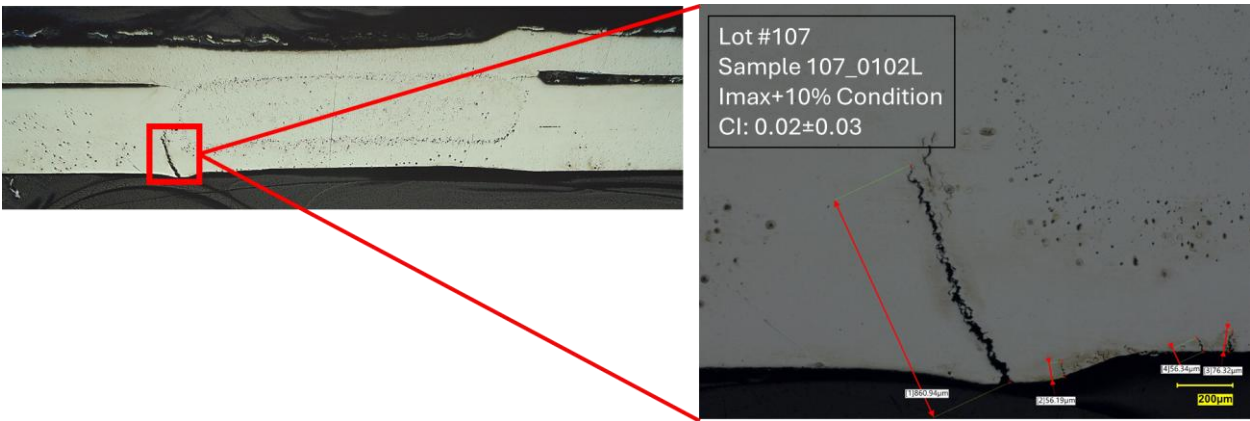
← Dissimilar stack-up



Similar Stack-up



Dissimilar Stack-up



# Conclusion of Task 1

- Using a Hierarchical evaluation process the following criteria were developed to results in the most industrially relevant LME characterization and testing methods:

|                                   | Type of metric | Definition of metric | Characterization method |
|-----------------------------------|----------------|----------------------|-------------------------|
| LME characterization alternatives | Quantitative   | Cracking index       | Cross-sectioning        |

|                          | stack-up          | welding current  |              | Electrode           | Nugget size | No. of tests |
|--------------------------|-------------------|------------------|--------------|---------------------|-------------|--------------|
| LME testing alternatives | Similar two-sheet | I <sub>max</sub> | Single-pulse | Based on a standard | Fixed       | More than 10 |

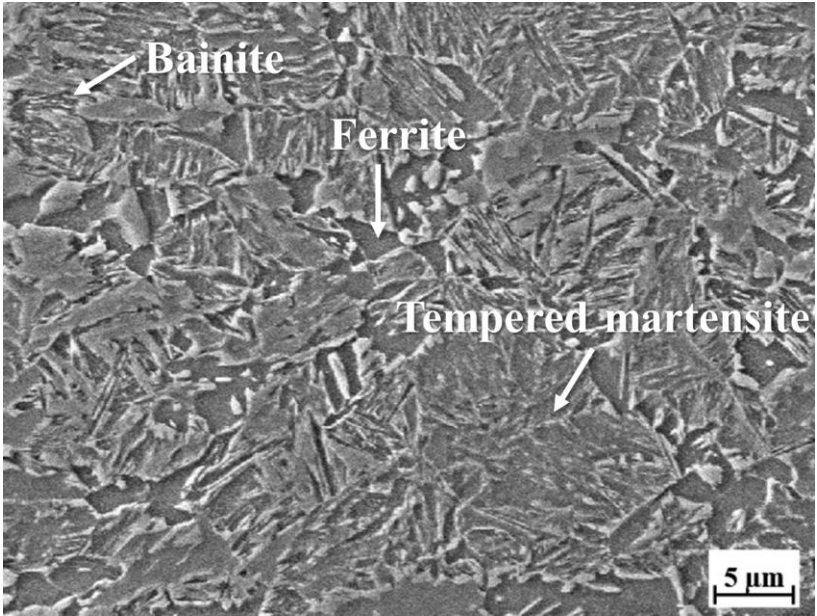
## Characterization:

- Maximum crack length exhibited a strong correlation with TSS data, but only a weak and inconsistent correlation with CTS
- Crack frequency and average crack length showed no significant correlation with either TSS or CTS.
- Cracking index (CI) demonstrated the strongest correlation with both TTS and CTS results.

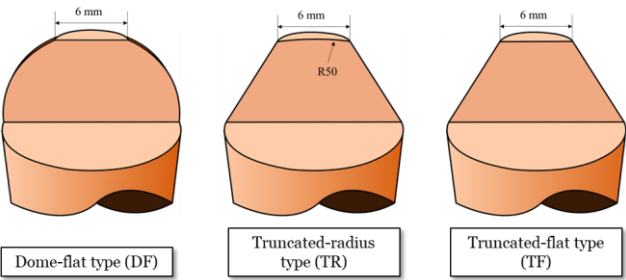
## Testing:

- Testing similar joints at currently levels 10% above the expulsion current resulted in the highest LME response with low variability
  - In a high LME susceptible very small cracks (<50 µm) dominated so the dissimilar joints with long cracks had a lower CI value than the similar joints

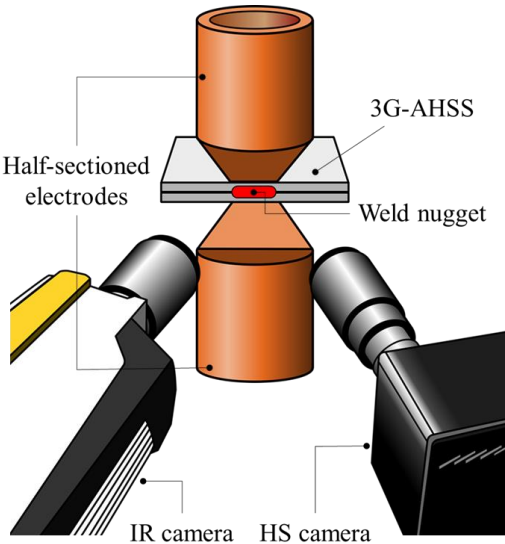
# Investigated Materials and Setup for Welds



|                 | C    | Mn + Si | Ti+Mo+V+Nb | C <sub>eq</sub> |
|-----------------|------|---------|------------|-----------------|
| GI- 980 3G-AHSS | 0.22 | 3.51    | 0.01       | 0.62            |

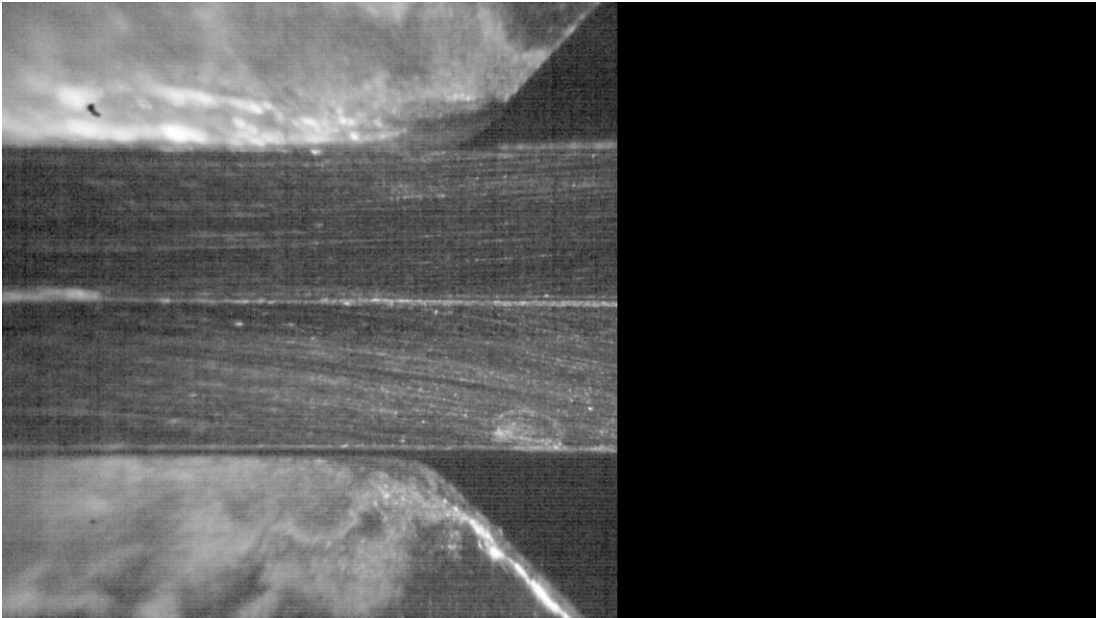


Schematic of H-RSW setup



| Half-sectioned welding parameter |                      |                   |                |                |                 |                                 |
|----------------------------------|----------------------|-------------------|----------------|----------------|-----------------|---------------------------------|
| Electrode Force (kN)             | Welding current (kA) | Squeeze time (ms) | Weld time (ms) | Hold time (ms) | Number of pulse | Cooling time between pulse (ms) |
| 2.16                             | 5.76                 | 394               | 200            | 167            | 2               | 33                              |

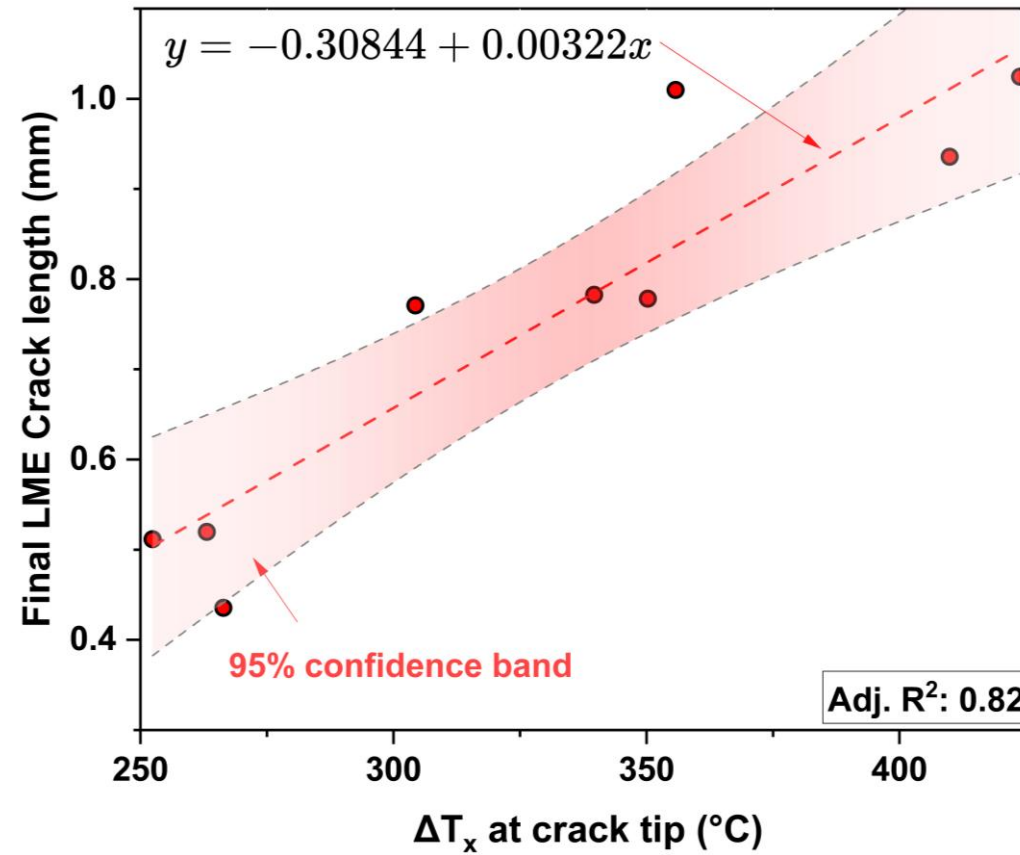
[Synchronized video]





# Prediction of LME Crack Length and Crack Growth Rate at Propagation Stage

Final LME crack length can be predicted based on the  $\Delta T_x$  at the tip

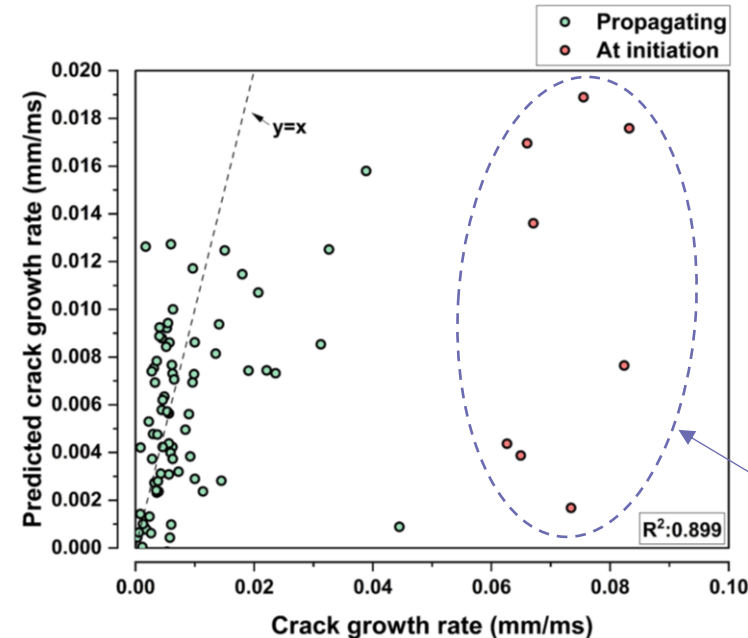


# Prediction of LME Crack Length and Crack Growth Rate at Propagation Stage

LME crack growth rate during **propagation** model, developed through multiple linear regression analysis, provides factors that control LME crack growth

$$\frac{dL}{dt} = \underbrace{\beta_1 \cdot \left(\frac{dL}{dt}\right)_{t-1}}_{\text{Crack's own momentum}} + \underbrace{\beta_2 \cdot \Delta T_x}_{\text{Thermal stress at the crack tip}} - \underbrace{\beta_3 \cdot \left(\frac{dL}{dt}\right)_{t-1} \cdot \Delta t}_{\text{Gradual reduction of thermal stress}} - \underbrace{\beta_4 \cdot \Delta T_x \cdot L_{i,j}}_{\text{Damping effects at the crack tip}}$$

Crack's own momentum    Damping effects at the crack tip



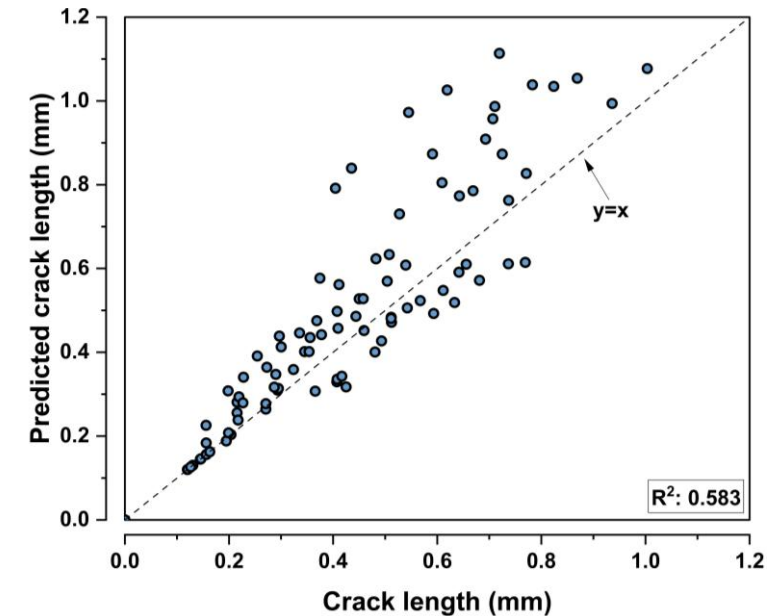
- $\beta_x$ : Coefficient of each term.
- $\left(\frac{dL}{dt}\right)_{t-1}$ : Crack growth rate at previous step.
- $\Delta T_x$ : Difference in temperature at crack tip.
- $\Delta t$ : Change in time.
- $L_{i,j}$ : Normalized LME crack length.

Data point related to the initiation stage

The LME crack length prediction model was developed using the LME crack growth rate model.

$$L = \underbrace{\left(\frac{dL}{dt}\right)_{t-1}}_{\text{predicted by the LME crack growth rate prediction model}} \cdot \Delta t + L_{t-1}$$

predicted by the LME crack growth rate prediction model



# Summary of LME Crack Initiation and Propagation

ITD Phenomenon due to electrode collapse generates thermal stress. This thermal stress promotes the diffusion of zinc into grain boundary



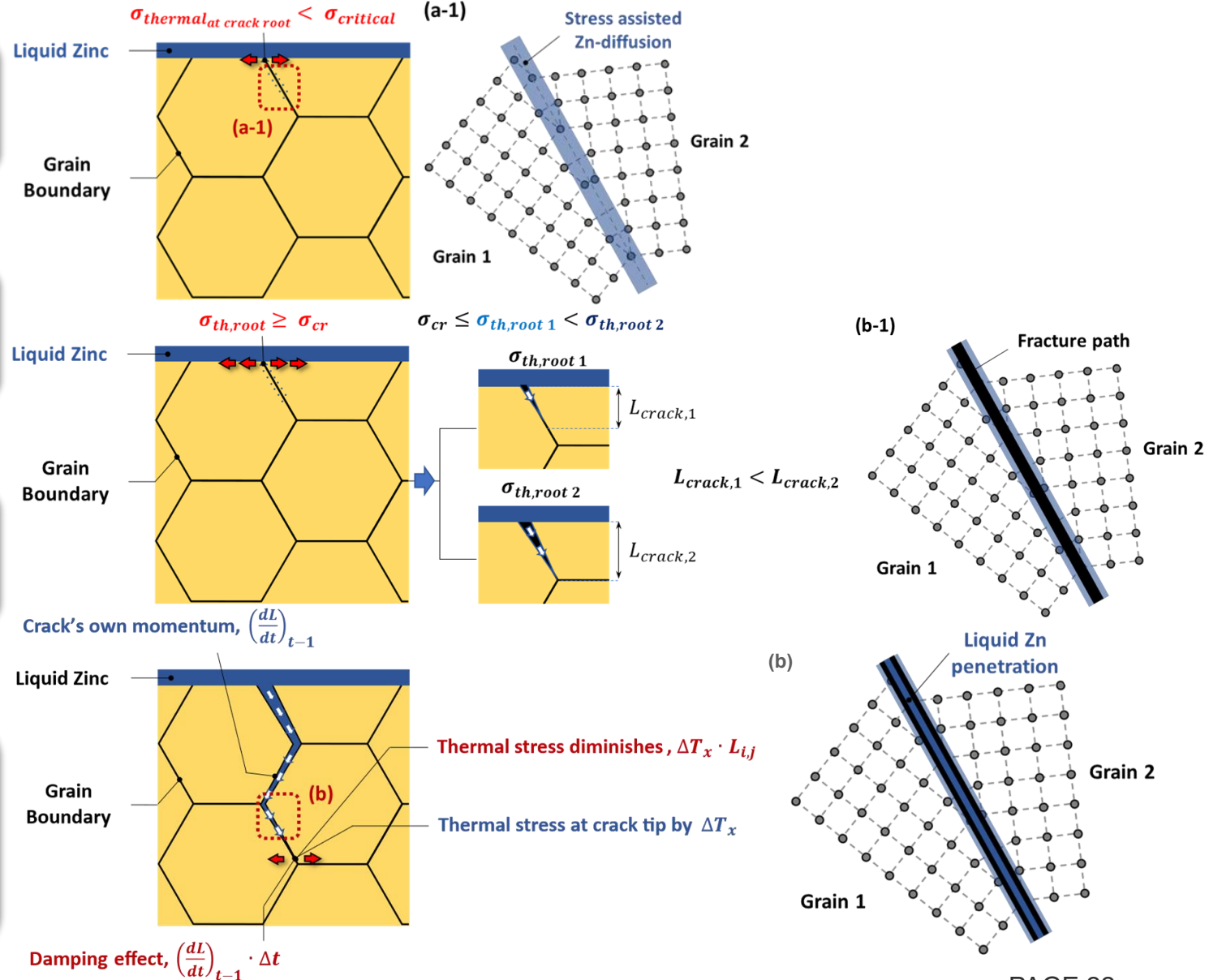
When thermal stress at crack root exceeds the critical threshold, LME crack initiate



At initiation stage, higher thermal stress leads to a longer crack length, and the fracture path develops along weakened grain boundaries



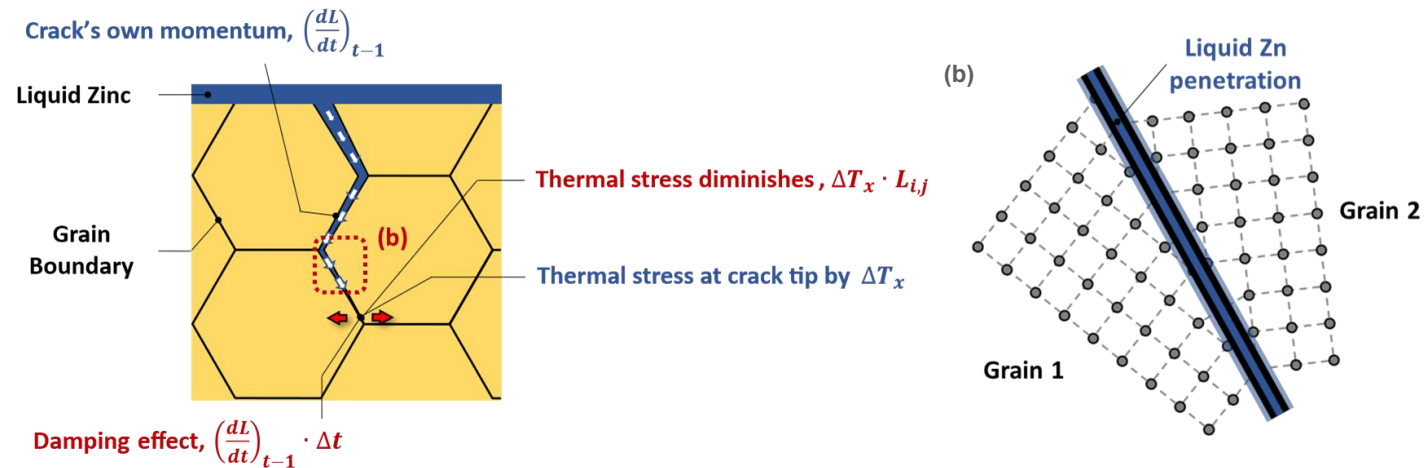
LME cracking behavior during propagation stage is characterized by four factors: the crack's own momentum, thermal stress at the crack tip, damping effect at the crack tip, and thermal stress reduction as the crack length increases



# Conclusion of Task 2

This study used real-time monitoring of LME cracking during actual spot-welding to quantify LME cracking behavior. This approach allowed for the determination of LME crack propagation kinetics and the development of models to predict crack length and growth rate.

- LME crack propagation is governed by the combined action of **four key factors**: the crack's momentum, thermal stress at the crack tip, damping effects at the crack tip, and gradual reduction of thermal stress as the crack length increases.



**Thanks for your attention!**